



File: 22249

FUNCTIONAL SERVICING REPORT

731 King Street, Niagara-On-The-Lake

April 2023

INTRODUCTION

The purpose of this report is to address the servicing needs for the proposed residential subdivision development in support of the applications for Zoning By-Law Amendment. The subject lands are located between 727 and 733 King Street in the Old Town Community of the Town of Niagara-on-the-Lake; north of King Street, west of Cottage Street, and south of Meritage Lane.

The development site is approximately 0.32 hectare and shall consist of 17 apartment units in a 3 storey building, and will include associated asphalt access and parking areas, concrete curb, catch basins, storm sewers, and sanitary sewers.

The objectives of this report are as follows:

1. Identify domestic and fire protection water servicing needs for the site;
2. Identify sanitary servicing needs for the site; and,
3. Identify stormwater management needs for the site.

WATER SERVICING

There is an existing municipal 150mm diameter watermain on King Street. It is proposed to connect a 150mm diameter water service to the existing 150mm watermain on King Street to provide both domestic water supply and fire protection. A private fire hydrant is required to provide fire protection, the location will be determined as part of the detailed engineering design.

Therefore, the existing water service on king Street will adequately provide domestic water supply and fire protection to the 17 unit building apartment.

SANITARY SERVICING

There is an existing 250mm diameter sanitary sewer on King Street which conveys sanitary flows to the northeast to Cottage Street. It is proposed to connect the new apartment building to the existing sanitary sewer on King Street and extend it within the site.

The proposed 0.32 hectare, 17 unit apartment building will produce a peak of approximately 0.91L/s, occupying 4.2% of the total capacity of the existing 250mm diameter sanitary sewer. Then, it is expected that this will be an adequate addition to the current capacity of the existing sanitary sewer.

STORMWATER MANAGEMENT

There are existing 450mm storm sewer on King Street, which convey stormwater flows southwest to Niagara Street, then southerly to Rye Street.

A Stormwater Drainage Area Plan was prepared in May 8, 2008 by Denco Engineering Ltd. (Denco) for the Town, as part of the King Street new storm sewer project, which delineated the storm drainage areas associated to the existing storm sewer system on King Street as shown in Appendix A.

In addition to the Stormwater Drainage Area Plan prepared by Denco Engineering, a new Stormwater Drainage Area plan was prepared by Upper Canada Consultants (UCC) as a part of the Royal Albion subdivision. As shown in the UCC plan attached in Appendix A, the storm drainage flows from the storm sewer on King Street, flow to Cottage Street and conveyed to the northwest towards Simcoe Street.

Figure 1, shows the Storm Drainage Areas from the original storm sewer design proposed by Denco where the 0.61 hectare with an associated Runoff Coefficient of 0.45 covers a portion. The original storm sewer calculations can be found in Appendix A.

The proposed and adjusted drainage areas and associated Runoff Coefficient is shown on Figure 2. The site stormwater system will collect a drainage area of 0.32 hectare at a Runoff Coefficient of 0.70. As shown in the proposed storm sewer calculation on Appendix A, the proposed conditions will produce a peak flow of 209.6 L/s, occupying 79.3% of the total capacity of the existing 450mm diameter storm sewer.

Therefore, since the majority the drainage areas A10 and A11 proposed by Denco will be conveyed to the existing Cottage Street storm sewer and the future proposed peak flows will be 11.0% less than the original peak flow proposed by Denco. It has been demonstrated that there will be adequate stormwater servicing capacity in the existing sewer network to serve the site without stormwater quantity controls.



To improve the quality of stormwater, an oil/grit separator will be utilized to provide MECP Normal Protection (70% TSS removal levels) as required for this type of development. It is estimated that a Hydroworks HD4 will provide 93% TSS removal. The complete stormwater design for this development will be identified as part of the future detailed design.

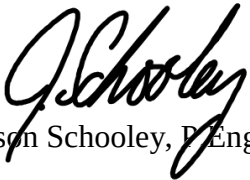
CONCLUSIONS AND RECOMMENDATIONS

Therefore, based on the above comments, drainage area plans and calculations provided for this site, the following summarizes the servicing for this site:

1. The existing 150mm diameter watermain on King Street is expected to have adequate capacity to provide both domestic water supply and fire protection to service the proposed 17 unit apartment building.
2. The receiving 250mm diameter sanitary sewers on King Street will have adequate capacity to service the Site.
3. The existing 450mm diameter stormwater sewer on King Street already has adequate capacity to serve the site.
4. Stormwater quality control will be provided to MECP Normal protection (70% TSS removal) levels prior to discharge from the site.

In conclusion, there exists adequate municipal servicing for this development. We trust the above comments and enclosed calculations are satisfactory for approval. If you have any questions or require additional information, please do not hesitate to contact our office.

Yours very truly,


Jason Schooley, P. Eng.



Encl.



**UPPER CANADA
CONSULTANTS**
ENGINEERS / PLANNERS

APPENDICES



**UPPER CANADA
CONSULTANTS**
ENGINEERS / PLANNERS

APPENDIX A

Drainage Area Plan, King Street, Denco Engineering Ltd.

Drainage Area Plan, Royal Albion Place, (UCC).

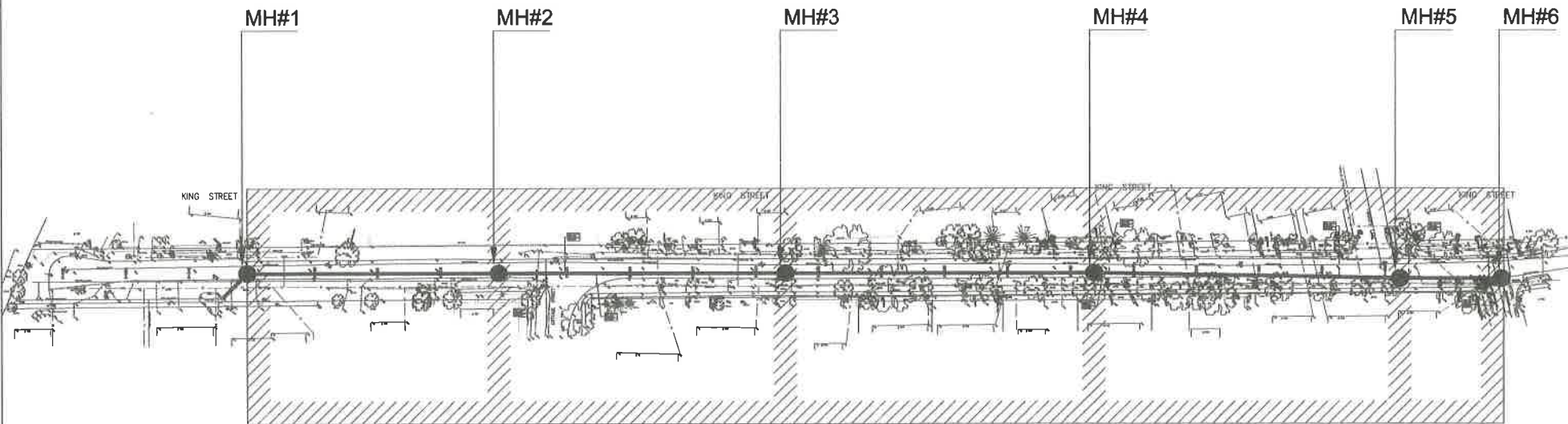
Figure 1. Existing Storm Drainage Area Plan.

Figure 2. Proposed Storm Drainage Area Plan.

Original Storm Sewer Design Sheet.

Proposed Storm Sewer Design Sheet.

Hydroworks – HydroDome Simulation.



SUB CATCHMENT AREA NUMBER	
RUNOFF COEFF.	AREA (ha.)

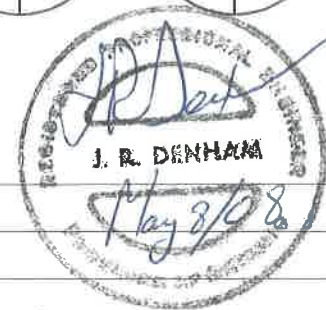
3	
0.45	0.60

2	
0.45	0.68

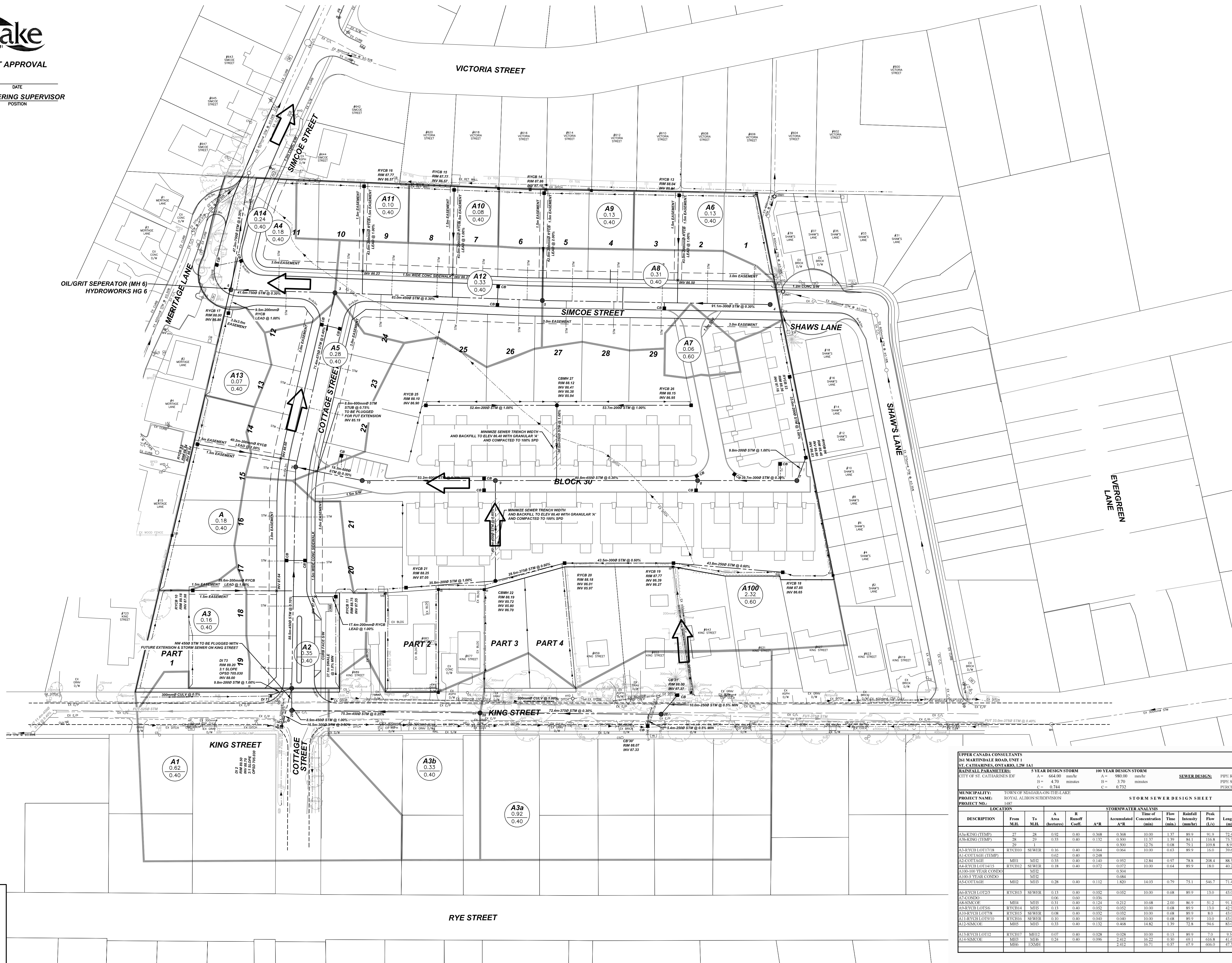
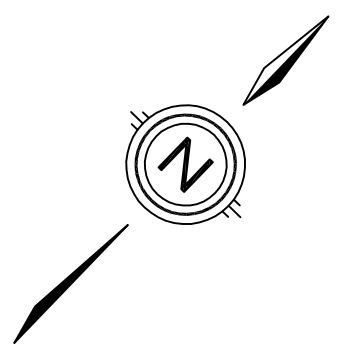
1	
0.45	0.73

4	
0.45	0.73

5	
0.45	0.25



1. DESIGN ADOPTED 2. REVISION		DATE: 05/03/08 BY: [Signature]	THE POSITION OF PUBLIC UTILITIES, CONDUITS, SEWERAGE, AND OTHER UNDERGROUND UTILITIES AND STRUCTURES IS NOT GUARANTEED. THE LOCATION OF THESE UTILITIES AND STRUCTURES IS BASED ON THE RECORD DRAWINGS AND FIELD SURVEY. THE LOCATION OF THESE UTILITIES AND STRUCTURES IS NOT GUARANTEED. THE LOCATION OF THESE UTILITIES AND STRUCTURES IS BASED ON THE RECORD DRAWINGS AND FIELD SURVEY.	DESIGNED BY: J.R.D. CHECKED BY: J.R.D. DATE: 05/03/08	TOWN OF NIAGARA ON THE LAKE DENCO 281 HARTSDALE ROAD, UNIT #17 ST. CATHARINES, ONTARIO (905) 641-3381 Fax: 641-5446	KING STREET STORM DRAINAGE AREA PLAN	FIELD NOTES: DATE: 05/14/07 SCALE: HORIZ. 1" = 200' VERT. 1" = 50' DATE: 05/03/08 BY: [Signature] 07014-DP
---	--	--	--	--	--	--	---



LEGEND

A0	DRAINAGE AREA NUMBER
0.00	DRAINAGE AREA IN HECTARES
0.00	RUN-OFF COEFFICIENT
	DRAINAGE AREA BOUNDARY
	OVERLAND FLOW ROUTE

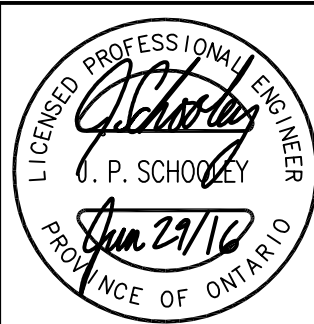
UPPER CANADA CONSULTANTS 261 Martindale Road Unit 1 St. Catharines, Ontario, L2M 1A1 Phone: (905) 688-9400 Fax: (905) 688-5274									
STORM SEWER DESIGN SHEET									
PROJECT NAME: ROYAL ALBION SUBDIVISION PROJECT NO.: 1487-STMDA									
STORMWATER ANALYSIS									
DESCRIPTION	From M.H.	To M.H.	A Area (hectares)	R Runoff Coeff.	A*R	Accumulated A*R	Time of Concentration (min)	Flow Time (min)	Rainfall Intensity (mm/hr)
AS-KING (TEMP)	27	28	0.32	0.40	0.128	0.128	10.00	1.37	89.9
AS-KING (TEMP)	28	29	0.33	0.40	0.132	0.260	11.57	1.39	84.1
AS-KING (TEMP)	29	1	0.40	0.40	0.160	0.420	12.76	0.68	79.1
AS-RYCH LOT17/18	RYCH10	SEWER	0.16	0.40	0.064	0.064	10.00	0.63	89.9
AS-COTTAGE (TEMP)	MEH	MEH	0.40	0.40	0.160	0.160	10.00	0.68	89.9
AS-COTTAGE (TEMP)	MEH	MEH	0.35	0.40	0.140	0.140	10.00	0.68	89.9
AS-RYCH LOT14/15	RYCH12	SEWER	0.18	0.40	0.072	0.072	10.00	0.64	89.9
AS-100 YEAR CONDO	MEH	MEH	0.33	0.40	0.132	0.132	10.00	0.68	89.9
AS-100 YEAR CONDO	MEH	MEH	0.28	0.40	0.112	0.112	10.00	0.75	75.1
AS-RYCH LOT12/13	RYCH13	SEWER	0.13	0.40	0.052	0.052	10.00	0.68	89.9
AS-CONDO	MEH	MEH	0.06	0.40	0.024	0.024	10.00	0.68	89.9
AS-SIMCOE	MEH	MEH	0.31	0.40	0.124	0.124	10.00	0.68	89.9
AS-RYCH LOT16/17	RYCH14	SEWER	0.13	0.40	0.052	0.052	10.00	0.68	89.9
AS-RYCH LOT17/18	RYCH15	SEWER	0.08	0.40	0.032	0.032	10.00	0.68	89.9
AS-RYCH LOT17/18	RYCH16	SEWER	0.10	0.40	0.040	0.040	10.00	0.68	89.9
AS-SIMCOE	MEH	MEH	0.33	0.40	0.132	0.132	10.00	0.68	89.9
AS-RYCH LOT12	RYCH17	SEWER	0.07	0.40	0.028	0.028	10.00	0.68	89.9
AS-SIMCOE	MEH	MEH	0.24	0.40	0.096	0.096	10.00	0.68	89.9
AS-SIMCOE	MEH	MEH	0.31	0.40	0.124	0.124	10.00	0.68	89.9

1	ISSUED FOR MOE APPROVAL	2016-06-29	M.C.
0	ISSUED FOR REVIEW	2016-04-27	M.C.
#	REVISION	DATE	INIT

NOTES/LEGEND

- THE POSITION OF POLE LINES, CONDUITS, WATERMANS, SEWER AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
- PROPERTY LINES WERE PLOTTED USING REGISTERED PLANS AND BARS LOCATED IN THE FIELD. TO VERIFY THE ACCURACY OF THESE PROPERTY LINES, A LEGAL SURVEY SHOULD BE PERFORMED PRIOR TO CONSTRUCTION.
- ALL CONSTRUCTION MUST COMPLY WITH THE NIAGARA PENINSULA STANDARD CONTRACT DOCUMENT.

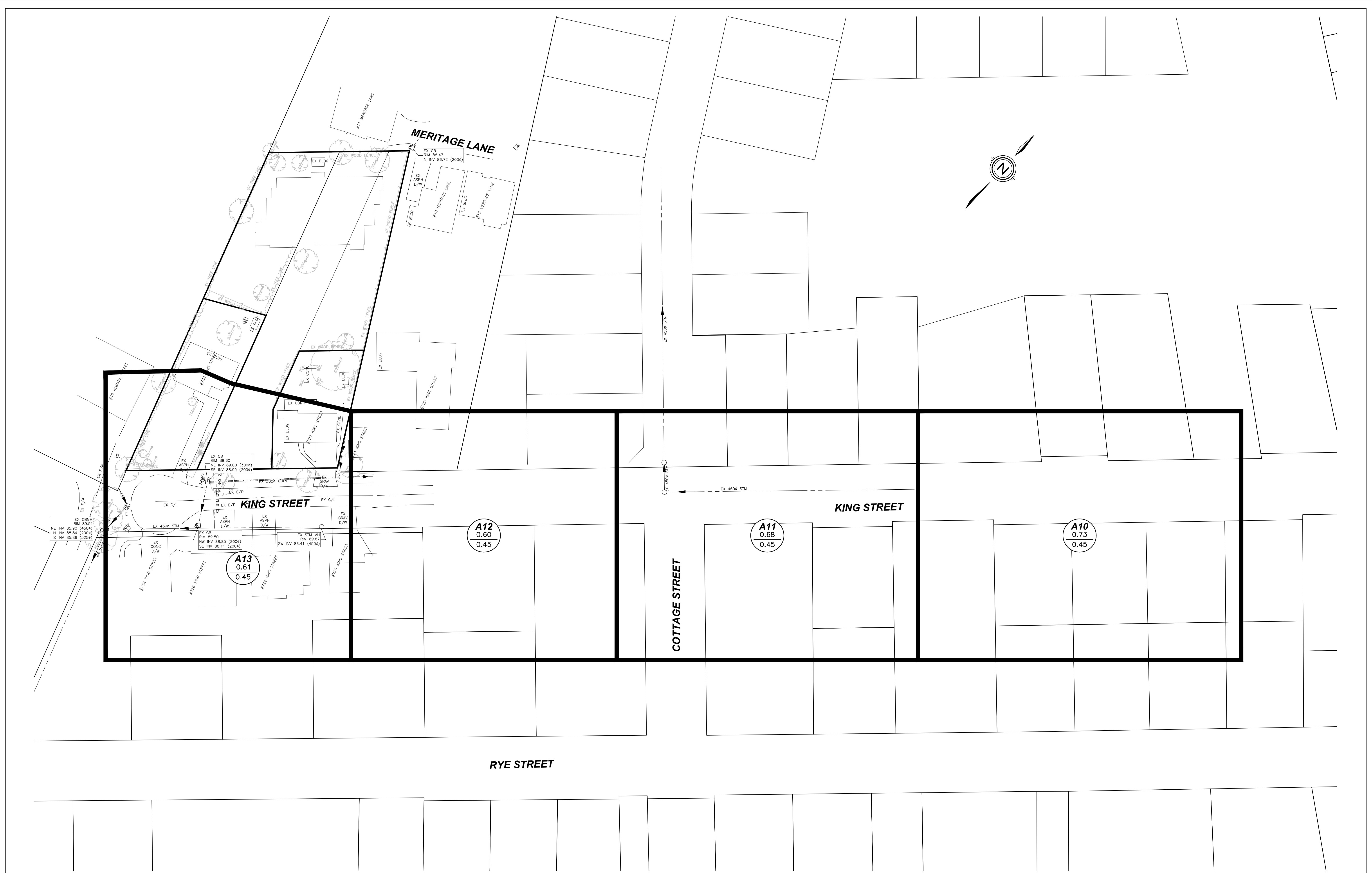
DRAFTING: MIKE C.
DESIGN: M.H./J.S.
CHECKED BY: J.S.
APPROVED BY: M.H.



OWNER: **GATTA HOMES INC.**
1624707 ONTARIO INC.

ROYAL ALBION PLACE
TOWN OF NIAGARA-ON-THE-LAKE
STORM DRAINAGE AREA PLAN

CONSULTANT FILE No. 1487
DATE: 2016-01-20
PRINTED: 2016-06-29
SCALE: Hor : 1:750 m
REF. No. _____
DWG No. **1487-STMDA**
REV. **1**



#	REVISION	DATE	INIT

NOTES:

1. THE POSITION OF POLE LINES, CONDUITS, WATERMANS, SEWER, AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
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3. ALL CONSTRUCTION MUST COMPLY WITH THE NIAGARA PENINSULA STANDARD CONTRACT DOCUMENT.

DRAFTING	
DESIGN	
CHECKED BY	
APPROVED BY	



UPPER CANADA
CONSULTANTS
ENGINEERS / PLANNERS

A0

0.00

0.00

DRAINAGE AREA NUMBER

DRAINAGE AREA IN HECTARES

RUN-OFF COEFFICIENT

DRAINAGE AREA BOUNDARY

OVERLAND FLOW ROUTE

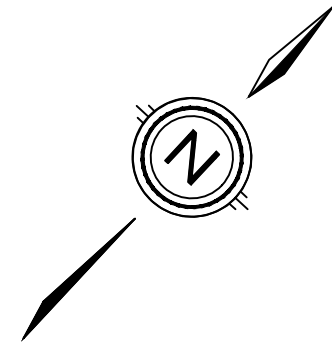
BICE APARTMENT

727-733 KING STREET

TOWN OF NIAGARA-ON-THE-LAKE

EXISTING STORM DRAINAGE PLAN

CONSULTANT FILE No. 22249	
DATE	2023-04-04
PRINTED	2023-04-11
SCALE	1:500 m
REF No.	
DWG No.	
REV	0
FIGURE 1	



#	REVISION	DATE	INIT

NOTES:

1. THE POSITION OF POLE LINES, CONDUITS, WATERMAINS, SEWER, AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
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3. ALL CONSTRUCTION MUST COMPLY WITH THE NIAGARA PENINSULA STANDARD CONTRACT DOCUMENT.

DRAFTING	
DESIGN	
CHECKED BY	
APPROVED BY	



UPPER CANADA
CONSULTANTS
ENGINEERS / PLANNERS

LEGEND

A0 0.00 0.00	DRAINAGE AREA NUMBER
	DRAINAGE AREA IN HECTARES
	RUN-OFF COEFFICIENT
	DRAINAGE AREA BOUNDARY
	OVERLAND FLOW ROUTE

BICE APARTMENT
727-733 KING STREET
TOWN OF NIAGARA-ON-THE-LAKE
FUTURE STORM DRAINAGE PLAN

CONSULTANT FILE No.	22249
DATE	2023-04-04
PRINTED	2023-04-06
SCALE	1:500 m
REF No.	
DWG No.	
REV	0

FIGURE 2

UPPER CANADA CONSULTANTS
3-30 HANNOVER DRIVE
ST. CATHARINES, ON L2W 1A3

<u>RAINFALL PARAMETERS:</u>	5 YEAR DESIGN STORM
CITY OF ST. CATHARINES IDF	A = 664.00 mm/hr
	B = 4.70 minutes
	C = 0.744

<u>SEWER DESIGN:</u>	PIPE ROUGHNESS:	0.013 FOR MANNING'S EQUATION
	PIPE SIZES:	1.016 ACTUAL DIAMETER SIZE FACTOR
	PERCENT FULL:	TOTAL PEAK FLOW / CAPACITY

MUNICIPALITY:	TOWN OF NIAGARA-ON-THE-LAKE
PROJECT NAME:	727-733 KING STREET
PROJECT NO.:	22249

ORIGINAL STORM SEWER DESIGN SHEET

[illegible]

UPPER CANADA CONSULTANTS
3-30 HANNOVER DRIVE
ST. CATHARINES, ON L2W 1A3

<u>RAINFALL PARAMETERS:</u>		5 YEAR DESIGN STORM				
CITY OF ST. CATHARINES IDF	A =	664.00	mm/hr	<u>SEWER DESIGN:</u>	PIPE ROUGHNESS:	0.013 FOR MANNING'S EQUATION
	B =	4.70	minutes		PIPE SIZES:	1.016 ACTUAL DIAMETER SIZE FACTOR
	C =	0.744			PERCENT FULL:	TOTAL PEAK FLOW / CAPACITY

MUNICIPALITY: TOWN OF NIAGARA-ON-THE-LAKE
PROJECT NAME: 727-733 KING STREET
PROJECT NO.: 22249

PROPOSED STORM SEWER DESIGN SHEET

PROPOSED STORM SEWER DESIGN SHEET

[illegible]

```

*****
*      Storm Water Management Sizing Model      *
*      Hydroworks, LLC                          *
*      Version 4.4                              *
*
*      Continuous Simulation Program             *
*      Based on SWMM 4.4H                       *
*      Hydroworks, LLC                          *
*      Graham Bryant                            *
*      2003 - 2021                              *
*****

```

Developed by

```

*****
*      Hydroworks, LLC                          *
*      Metcalf & Eddy, Inc.                     *
*      University of Florida                     *
*      Water Resources Engineers, Inc.           *
*      (Now Camp Dresser & McKee, Inc.)          *
*      Modified SWMM 4.4                        *
*****

```

Distributed and Maintained by

```

*****
*      Hydroworks, LLC                          *
*      888-290-7900                             *
*      www.hydroworks.com                       *
*****

```

```

*****
*      If any problems occur executing this     *
*      model, contact Mr. Graham Bryant at      *
*      Hydroworks, LLC by phone at 888-290-7900 *
*      or by e-mail: support@hydroworks.com     *
*****

```

```

*****
*      This model is based on EPA SWMM 4.4      *
*      "Nature is full of infinite causes which *
*      have never occurred in experience" da Vinci *
*****

```

```

*****
*      Entry made to the Rain Block              *
*      Created by the University of Florida - 1988 *
*      Updated by Oregon State University, March 2000 *
*****

```

727 - 733 KING STREET
 NIAGRA ON THE LAKE

HydroDome Simulation

```

#####
# Precipitation Block Input Commands #
#####

```

```

Station Name..... St. Catherines A
Station Location..... Ontario
Station, ISTA..... 7287
Beginning date, IYBEG (Yr/Mo/Dy)..... 1971/ 1/ 1
Ending date, IYEND (Yr/Mo/Dy)..... 2005/12/31
Minimum interevent time, MIT..... 1
Number of ranked storms, NPTS..... 10
NWS format, IFORM (See text)..... 1
Print storm summary, ISUM (0-No 1-Yes) 0
Print all rainfall, IYEAR (0-No 1-Yes) 0
Save storm event data on NSCRAT(1).... 0
(IFILE =0 -Do not save, =1 -Save data)
IDECID 0 - Create interface file
      1 - Create file and analyze
      2 - Synoptic analysis..... 2
Plotting position parameter, A..... 0.40
Storm event statistics, NOSTAT..... 1100

```

```

KODEA (from optional group B0)..... 2
= 0, Do not include NCDC cumulative values.
= 1, Average NCDC cumulative values.
= 2, Use NCDC cumulative value as inst. rain.

```

```

KODEPR (from optional group B0)..... 0
Print NCDC special codes in event summary:
= 0, only on days with events.
= 1, on all days with codes present.
Codes: A = accumulated value, I = incomplete value,
      M = missing value,      O = other code present

```


SUBCATCHMENT NO.	CHANNEL OR INLET	WIDTH (M)	AREA (HA)	PERCENT IMPERV.	SLOPE (M/M)	RESISTANCE IMPERV.	FACTOR PERV.	DEPRES. IMPERV.	STORAGE (MM) PERV.	INFILTRATION RATE (MM/HR)		DECAY RATE (1/SEC)	GAGE NO.	MAXIMUM VOLUME (MM)	
										MAXIMUM	MINIMUM				
1	300	200	56.57	0.32	71.42	0.0200	0.015	0.250	0.510	5.080	63.50	10.16	0.00055	1	101.6000

TOTAL NUMBER OF SUBCATCHMENTS... 1
TOTAL TRIBUTARY AREA (HECTARES)... 0.32
IMPERVIOUS AREA (HECTARES)..... 0.23
PERVIOUS AREA (HECTARES)..... 0.09
TOTAL WIDTH (METERS)..... 56.57
PERCENT IMPERVIOUSNESS..... 71.42

* G R O U N D W A T E R I N P U T D A T A *

SUB- CATCH NUMBER	CHANNEL OR INLET	===== E L E V A T I O N S =====	===== F L O W C O N S T A N T S =====
		GROUND (M) BOTTOM (M) STAGE (M) BC (M) TW (M) A1 (MM/HR-M^B1) B1 A2 (MM/HR-M^B2) B2 A3 (MM/HR-M^2)	
0	602	3.05 0.00 0.00 0.61 0.61 3.484E-04	2.600 0.000E+00 1.000 0.00E+00

* G R O U N D W A T E R I N P U T D A T A (CONTINUED) *

SUBCAT. NO.	POROSITY	SATURATED HYDRAULIC CONDUCTIVITY (mm/hr)	WILTING POINT	FIELD CAPACITY	INITIAL MOISTURE	MAX. DEEP PERCOLATION (mm/hr)	PERCOLATION HCO	PARAMETERS PCO	ET OF ET (m)	DEPTH TO UPPER ZONE	FRACTION OF ET
0	.4000	127.000	.1500	.3000	.3000	5.080E-02	10.00	4.57	4.27	0.350	

* Arrangement of Subcatchments and Channel/Pipes *

* See second subcatchment output table for connectivity *
* of subcatchment to subcatchment flows. *

Channel
or Pipe
201 No Tributary Channel/Pipes
No Tributary Subareas.....

INLET
200 Tributary Channel/Pipes... 201
Tributary Subareas..... 300

* Hydrographs will be stored for the following 1 INLETS *

200

Quality Simulation #

General Quality Control Data Groups #
#####

Description	Variable	Value
Number of quality constituents....	NQS.....	1
Number of land uses.....	JLAND.....	1
Standard catchbasin volume.....	CBVOL.....	1.22 cubic meters
Erosion is not simulated.....	IROS.....	0
DRY DAYS PRIOR TO START OF STORM...	DRYDAY.....	3.00 DAYS
DRY DAYS REQUIRED TO RECHARGE		
CATCHBASIN CONCENTRATION TO		
INITIAL VALUES.....	DRYBSN.....	5.00 DAYS
DUST AND DIRT		
STREET SWEEPING EFFICIENCY.....	REFFDD.....	0.300
DAY OF YEAR ON WHICH STREET		
SWEEPING BEGINS.....	KLNBGN.....	120
DAY OF YEAR ON WHICH STREET		
SWEEPING ENDS.....	KLNEND.....	270

Land use data on data group J2 #
#####

AND USE LNAME)	BUILDUP EQUATION TYPE (METHOD)	FUNCTIONAL DEPENDENCE OF BUILDUP PARAMETER (JACGUT)	LIMITING BUILDUP QUANTITY (DDLIM)	BUILDUP POWER (DDPOW)	BUILDUP COEFF. (DDFACT)	CLEANING INTERVAL IN DAYS (CLFREQ)	AVAIL. FACTOR (AVSWP)	DAYS SINCE LAST SWEEPING (DSLCL)
Urban De	EXPONENTIAL(1)	AREA(1)	2.802E+01	0.500	67.250	30.000	0.300	30.000

```
#####
#      Constituent data on data group J3      #
#####
```

```

Total Su
-----
Constituent units..... mg/l
Type of units..... 0
KALC..... 2
Type of buildup calc.... EXPONENTIAL(2)
KWASH..... 0
Type of washoff calc.... POWER EXPONEN.(0)
KACGUT..... 1
Dependence of buildup... AREA(1)
LINKUP..... 0
Linkage to snowmelt..... NO SNOW LINKAGE
Buildup param 1 (QFACT1).. 28.020
Buildup param 2 (QFACT2).. 0.500
Buildup param 3 (QFACT3).. 67.250
Buildup param 4 (QFACT4).. 0.000
Buildup param 5 (QFACT5).. 0.000
Washoff power (WASHPO)... 1.100
Washoff coef. (RCOEF)... 0.086
Init catchb conc (CBFACT) 100.000
Precip. conc. (CONCRN)... 0.000
Street sweep effic (REFF) 0.300
Remove fraction (REMOVE).. 0.000
1st order QDECAV, 1/day.. 0.000
Land use number..... 1

```

```
*****
* Constant Groundwater Quality Concentration(s) *
*****
```

Total Susp has a concentration of.. 0.0000 mg/l

```
*****
* REMOVAL FRACTIONS FOR SELECTED CHANNEL/PIPES *
* FROM J7 LINES *
*****
```

```

CHANNEL/  CONSTITUENT
PIPE Total Susp
-----
201      0.000

```

```
*****
* Subcatchment surface quality on data group L1 *
*****
```

	Land No. Usage	Land Use No.	Total Gutter Length Km	Number of Catch- Basins	Input Loading load/ha Total Su
1	300 Urban De	1	0.11	2.00	0.0E+00
Totals (Loads in kg or other)			0.11	2.00	0.0E+00

```
*****
* DATA GROUP M1 *
*****
```

```
TOTAL NUMBER OF PRINTED GUTTERS/INLETS...NPRNT.. 1
NUMBER OF TIME STEPS BETWEEN PRINTINGS...INTERV.. 0
STARTING AND STOPPING PRINTOUT DATES..... 0 0
```

```
*****
* DATA GROUP M3 *
*****
```

CHANNEL/INLET PRINT DATA GROUPS..... -200

```
*****
* Rainfall from Nat. Weather Serv. file *
* in units of hundredths of an inch *
*****
```

Rainfall Station St. Catherines A
State/Province Ontario

Rainfall Depth Summary (mm)

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
1971.	31.	0.	0.	0.	0.	0.	126.	93.	52.	60.	29.	0.	391.
1972.	0.	0.	0.	47.	65.	100.	39.	115.	63.	90.	1.	0.	521.
1973.	0.	0.	0.	103.	77.	71.	53.	29.	63.	139.	0.	0.	534.
1974.	0.	0.	0.	67.	105.	62.	50.	31.	74.	37.	110.	0.	536.
1975.	0.	0.	0.	0.	0.	94.	78.	76.	73.	56.	59.	6.	442.
1976.	0.	0.	0.	119.	136.	87.	101.	60.	72.	73.	13.	1.	662.
1977.	0.	0.	0.	94.	29.	69.	57.	150.	230.	71.	0.	1.	701.
1978.	0.	0.	0.	72.	43.	72.	43.	86.	156.	95.	0.	0.	567.

1979.	0.	0.	0.	84.	92.	33.	91.	88.	84.	129.	71.	0.	673.
1980.	0.	0.	0.	81.	39.	122.	60.	32.	79.	96.	45.	0.	554.
1981.	0.	0.	0.	91.	71.	106.	122.	61.	123.	91.	84.	0.	749.
1982.	0.	0.	0.	28.	65.	97.	36.	66.	82.	25.	143.	0.	544.
1983.	0.	0.	0.	78.	100.	65.	55.	106.	75.	122.	92.	0.	694.
1984.	0.	0.	0.	31.	113.	136.	19.	51.	144.	24.	44.	0.	562.
1985.	0.	0.	67.	32.	52.	64.	40.	94.	42.	109.	0.	1.	501.
1986.	0.	0.	0.	93.	113.	60.	85.	83.	98.	80.	43.	65.	719.
1987.	0.	2.	11.	77.	42.	80.	122.	97.	99.	71.	94.	34.	730.
1988.	0.	0.	41.	71.	42.	21.	110.	82.	70.	68.	75.	5.	585.
1989.	0.	0.	13.	63.	137.	108.	36.	45.	89.	73.	84.	0.	647.
1990.	0.	2.	38.	99.	124.	44.	68.	95.	56.	112.	96.	0.	735.
1991.	0.	0.	86.	124.	67.	31.	85.	57.	79.	64.	61.	28.	682.
1992.	0.	0.	29.	127.	56.	92.	185.	116.	77.	47.	103.	38.	869.
1993.	3.	0.	7.	83.	56.	86.	32.	61.	71.	92.	80.	38.	610.
1994.	0.	0.	44.	88.	105.	124.	48.	77.	117.	15.	0.	15.	633.
1995.	112.	23.	16.	48.	37.	60.	123.	66.	8.	137.	94.	0.	724.
1998.	0.	0.	0.	0.	51.	54.	64.	29.	9.	0.	1.	0.	207.
1999.	0.	0.	0.	79.	59.	35.	61.	58.	116.	78.	0.	0.	487.
2000.	0.	0.	0.	123.	134.	216.	51.	0.	0.	0.	10.	0.	534.
2001.	0.	0.	0.	56.	88.	45.	25.	30.	81.	129.	0.	0.	454.
2002.	0.	0.	0.	73.	104.	64.	53.	49.	52.	65.	8.	0.	468.
2003.	0.	0.	0.	10.	163.	77.	81.	64.	67.	73.	2.	0.	537.
2004.	0.	0.	0.	131.	126.	99.	115.	40.	88.	17.	0.	0.	616.
2005.	0.	0.	0.	38.	42.	78.	53.	120.	112.	0.	0.	0.	443.

Total Rainfall Depth for Simulation Period 19310. (mm)

Rainfall Intensity Analysis (mm/hr)

(mm/hr)	(#)	(%)	(mm)	(%)
2.50	21481	74.6	6454.	33.4
5.00	3585	12.4	3088.	16.0
7.50	1973	6.8	2886.	14.9
10.00	575	2.0	1233.	6.4
12.50	389	1.4	1070.	5.5
15.00	194	0.7	660.	3.4
17.50	210	0.7	846.	4.4
20.00	66	0.2	306.	1.6
22.50	92	0.3	487.	2.5
25.00	39	0.1	232.	1.2
27.50	37	0.1	246.	1.3
30.00	34	0.1	245.	1.3
32.50	29	0.1	228.	1.2
35.00	5	0.0	42.	0.2
37.50	10	0.0	90.	0.5
40.00	10	0.0	97.	0.5
42.50	12	0.0	124.	0.6
45.00	9	0.0	99.	0.5
47.50	1	0.0	12.	0.1
50.00	3	0.0	37.	0.2
>50.00	49	0.2	829.	4.3

Total # of Intensities 28803

Daily Rainfall Depth Analysis (mm)

(mm)	(#)	(%)	(mm)	(%)
2.50	1077	38.9	1247.	6.5
5.00	507	18.3	1850.	9.6
7.50	326	11.8	2006.	10.4
10.00	226	8.2	1958.	10.1
12.50	150	5.4	1672.	8.7
15.00	111	4.0	1495.	7.7
17.50	100	3.6	1620.	8.4
20.00	67	2.4	1260.	6.5
22.50	45	1.6	958.	5.0
25.00	37	1.3	881.	4.6
27.50	23	0.8	609.	3.2
30.00	20	0.7	575.	3.0
32.50	20	0.7	631.	3.3
35.00	12	0.4	405.	2.1
37.50	8	0.3	290.	1.5
40.00	9	0.3	350.	1.8
42.50	4	0.1	165.	0.9
45.00	4	0.1	173.	0.9
47.50	2	0.1	91.	0.5
50.00	4	0.1	192.	1.0
>50.00	15	0.5	882.	4.6

Total # Days with Rain 2767

 * End of time step DO-loop in Runoff *

Final Date (Mo/Day/Year)	=	1/ 1/2006
Total number of time steps	=	2056358
Final Julian Date	=	2006001
Final time of day	=	2. seconds.
Final time of day	=	0.00 hours.
Final running time	=	306816.0000 hours.
Final running time	=	12784.0000 days.

```

*****
*   Extrapolation Summary for Watersheds   *
* # Steps ==> Total Number of Extrapolated Steps *
* # Calls ==> Total Number of OVERLND Calls *
*****

```

Subcatch	# Steps	# Calls	Subcatch	# Steps	# Calls	Subcatch	# Steps	# Calls
-----	-----	-----	-----	-----	-----	-----	-----	-----
300	6155517	1559211						

```

*****
*   Extrapolation Summary for Channel/Pipes *
* # Steps ==> Total Number of Extrapolated Steps *
* # Calls ==> Total Number of GUTNR Calls *
*****

```

Chan/Pipe	# Steps	# Calls	Chan/Pipe	# Steps	# Calls	Chan/Pipe	# Steps	# Calls
-----	-----	-----	-----	-----	-----	-----	-----	-----
201	0	0						

```

*****
*   Continuity Check for Surface Water   *
*****

```

	cubic meters	Millimeters over Total Basin
Total Precipitation (Rain plus Snow)	61640.	19263.
Total Infiltration	17516.	5474.
Total Evaporation	4316.	1349.
Surface Runoff from Watersheds	40288.	12590.
Total Water remaining in Surface Storage	0.	0.
Infiltration over the Pervious Area...	17516.	19152.

Infiltration + Evaporation +		
Surface Runoff + Snow removal +		
Water remaining in Surface Storage +		
Water remaining in Snow Cover.....	62119.	19413.
Total Precipitation + Initial Storage.	61640.	19263.

The error in continuity is calculated as

```

*****
* Precipitation + Initial Snow Cover *
* - Infiltration - *
*Evaporation - Snow removal - *
*Surface Runoff from Watersheds - *
*Water in Surface Storage - *
*Water remaining in Snow Cover *
*-----*
* Precipitation + Initial Snow Cover *
*****
Error..... -0.778 Percent

```

```

*****
*   Continuity Check for Channel/Pipes   *
*****

```

	cubic meters	Millimeters over Total Basin
Initial Channel/Pipe Storage.....	0.	0.
Final Channel/Pipe Storage.....	0.	0.
Surface Runoff from Watersheds.....	40288.	12590.
Baseflow.....	0.	
Groundwater Subsurface Inflow.....	0.	0.
Evaporation Loss from Channels.....	0.	0.
Channel/Pipe/Inlet Outflow.....	40288.	12590.
Initial Storage + Inflow.....	40288.	12590.
Final Storage + Outflow.....	40288.	12590.

* Final Storage + Outflow + Evaporation - *		
* Watershed Runoff - Groundwater Inflow - *		
* Initial Channel/Pipe Storage *		
* ----- *		
* Final Storage + Outflow + Evaporation *		

Error..... 0.000 Percent		

```

*****
*   Continuity Check for Subsurface Water *
*****

```

	cubic meters	Millimeters over Subsurface Basin
Total Infiltration	0.	0.
Total Upper Zone ET	0.	0.
Total Lower Zone ET	0.	0.
Total Groundwater flow	0.	0.
Total Deep percolation	0.	0.
Initial Subsurface Storage	2926.	914.
Final Subsurface Storage	2926.	914.
Upper Zone ET over Pervious Area	0.	0.
Lower Zone ET over Pervious Area	0.	0.

```

*****
* Infiltration + Initial Storage - Final *
* Storage - Upper and Lower Zone ET - *
* Groundwater Flow - Deep Percolation *
* ----- *
* Infiltration + Initial Storage *
*****
Error ..... 0.000 Percent

```

SUMMARY STATISTICS FOR SUBCATCHMENTS =====

SUBCATCH- MENT NO.	GUTTER OR INLET NO.	AREA (HA)	PERCENT IMPER.	TOTAL SIMULATED RAINFALL (MM)	PERVIOUS AREA			IMPERVIOUS AREA		TOTAL SUBCATCHMENT AREA		
					TOTAL DEPTH (MM)	TOTAL LOSSES (MM)	PEAK RUNOFF (CMS)	RUNOFF DEPTH (MM)	PEAK RUNOFF (CMS)	RUNOFF DEPTH (MM)	PEAK RUNOFF (CMS)	PEAK UNIT RUNOFF (MM/HR)
300	200	0.32	71.419262	47	113.458	*****	0.03317580	303	0.124	12588.278	0.158	178.977

*** NOTE *** IMPERVIOUS AREA STATISTICS AGGREGATE IMPERVIOUS AREAS WITH AND WITHOUT DEPRESSION STORAGE

SUMMARY STATISTICS FOR CHANNEL/PIPES =====

CHANNEL NUMBER	FULL FLOW (CMS)	FULL VELOCITY (M/S)	FULL DEPTH (M)	MAXIMUM COMPUTED INFLOW (CMS)	MAXIMUM COMPUTED OUTFLOW (CMS)	MAXIMUM COMPUTED DEPTH (M)	MAXIMUM COMPUTED VELOCITY (M/S)	TIME OF OCCURRENCE DAY HR.	LENGTH OF SURCHARGE (HOUR)	MAXIMUM SURCHARGE VOLUME (CU-M)	RATIO OF MAX. TO FULL FLOW	RATIO OF MAX. DEPTH TO FULL DEPTH
201				0.00				1/ 0/1900	0.00			
200				0.16				8/14/1972	14.25			

TOTAL NUMBER OF CHANNELS/PIPES = 2

*** NOTE *** THE MAXIMUM FLOWS AND DEPTHS ARE CALCULATED AT THE END OF THE TIME INTERVAL

```

#####
# Runoff Quality Summary Page #
# If NDIM = 0 Units for: loads mass rates #
# METRIC = 1 lb lb/sec #
# METRIC = 2 kg kg/sec #
# If NDIM = 1 Loads are in units of quantity #
# and mass rates are quantity/sec #
# If NDIM = 2 loads are in units of concentration #
# times volume and mass rates have units#
# of concentration times volume/second #
#####

```

Total Su NDIM = 0
METRIC = 2

Total Su

Inputs -----

```

1. INITIAL SURFACE LOAD..... 7.
2. TOTAL SURFACE BUILDUP..... 5642.
3. INITIAL CATCHBASIN LOAD..... 0.
4. TOTAL CATCHBASIN LOAD..... 0.
5. TOTAL CATCHBASIN AND
   SURFACE BUILDUP (2+4)..... 5642.

```

Remaining Loads -----

```

6. LOAD REMAINING ON SURFACE... 3.
7. REMAINING IN CATCHBASINS.... 0.
8. REMAINING IN CHANNEL/PIPES.. 0.

```

Removals -----

```

9. STREET SWEEPING REMOVAL..... 473.
10. NET SURFACE BUILDUP (2-9)... 5169.
11. SURFACE WASHOFF..... 5166.
12. CATCHBASIN WASHOFF..... 0.
13. TOTAL WASHOFF (11+12)..... 5166.
14. LOAD FROM OTHER CONSTITUENTS 0.
15. PRECIPITATION LOAD..... 0.
15a. SUM SURFACE LOAD (13+14+15). 5166.
16. TOTAL GROUNDWATER LOAD..... 0.
16a. TOTAL I/I LOAD..... 0.
17. NET SUBCATCHMENT LOAD
   (15a-15b-15c-15d+16+16a).... 5166.
>>Removal in channel/pipes (17a, 17b):
17a.REMOVE BY BMP FRACTION..... 0.
17b.REMOVE BY 1st ORDER DECAY... 0.
18. TOTAL LOAD TO INLETS..... 5166.
19. FLOW WT'D AVE.CONCENTRATION mg/l
   (INLET LOAD/TOTAL FLOW)..... 128.

```

Percentages

20. STREET SWEEPING (9/2).....	8.
21. SURFACE WASHOFF (11/2).....	92.
22. NET SURFACE WASHOFF(11/10)..	100.
23. WASHOFF/SUBCAT LOAD(11/17)..	100.
24. SURFACE WASHOFF/INLET LOAD (11/18).....	100.
25. CATCHBASIN WASHOFF/ SUBCATCHMENT LOAD (12/17)...	0.
26. CATCHBASIN WASHOFF/ INLET LOAD (12/18).....	0.
27. OTHER CONSTITUENT LOAD/ SUBCATCHMENT LOAD (14/17)...	0.
28. INSOLUBLE FRACTION/ INLET LOAD (14/18).....	0.
29. PRECIPITATION/ SUBCATCHMENT LOAD (15/17)...	0.
30. PRECIPITATION/ INLET LOAD (15/18).....	0.
31. GROUNDWATER LOAD/ SUBCATCHMENT LOAD (16/17)...	0.
32. GROUNDWATER LOAD/ INLET LOAD (16/18).....	0.
32a.INFILTRATION/INFLOW LOAD/ SUBCATCHMENT LOAD (16a/17)..	0.
32b.INFILTRATION/INFLOW LOAD/ INLET LOAD (16a/18).....	0.
32c.CH/PIPE BMP FRACTION REMOVAL/ SUBCATCHMENT LOAD (17a/17)..	0.
32d.CH/PIPE 1st ORDER DECAY REMOVAL/ SUBCATCHMENT LOAD (17b/17)..	0.
33. INLET LOAD SUMMATION ERROR (18+8+6a+17a+17b-17)/17.....	0.

CAUTION. Due to method of quality routing (Users Manual, Appendix IX) quality routing through channel/pipes is sensitive to the time step. Large "Inlet Load Summation Errors" may result. These can be reduced by adjusting the time step(s). Note: surface accumulation during dry time steps at end of simulation is not included in totals. Buildup is only performed at beginning of wet steps or for street cleaning.

* TSS Particle Size Distribution *				

Diameter	%	Specific	Settling Velocity	Critical Peclet
(um)		Gravity	(m/s)	Number
20.	20.0	2.65	0.000267	0.080977
60.	20.0	2.65	0.002319	0.160673
150.	20.0	2.65	0.012234	0.284537
400.	20.0	2.65	0.047806	0.524584
2000.	20.0	2.65	0.180097	1.431405

*****		*
* Summary of TSS Removal		*
*****		*

TSS Removal based on Lab Performance Curve

Model #	Low Q Treated (cms)	High Q Treated (cms)	Runoff Treated (%)	TSS Removed (%)
Unavailabl	0.056	0.056	99.7	89.3
HD 4	0.056	0.056	99.7	93.1
HD 5	0.056	0.056	99.7	95.7
HD 6	0.056	0.056	99.7	97.5
Unavailabl	0.056	0.056	99.7	98.4
HD 8	0.056	0.056	99.7	98.9
HD 10	0.056	0.056	99.7	99.4
HD 12	0.056	0.056	99.7	99.7

*****		*
* Summary of Annual Flow Treatmnet & TSS Removal		*
*****		*

Unavailabl Year	Flow Vol (m3)	Flow Treated (m3)	TSS In (kg)	TSS Rem (kg)	TSS Out (kg)	TSS Byp (kg)	Flow Treated (%)	TSS Removal (%)
1971.	4210.	4195.	102.	88.	14.	0.	99.7	86.2
1972.	5414.	5025.	134.	120.	13.	4.	92.8	87.3
1973.	5371.	5371.	144.	129.	15.	0.	100.0	89.7
1974.	5486.	5468.	154.	142.	12.	0.	99.7	92.1
1975.	4647.	4647.	132.	116.	16.	0.	100.0	87.9
1976.	6916.	6849.	165.	149.	16.	1.	99.0	89.5
1977.	7413.	7320.	161.	136.	25.	1.	98.7	84.0
1978.	5913.	5913.	153.	133.	20.	0.	100.0	87.1
1979.	7080.	7031.	176.	158.	18.	0.	99.3	89.3
1980.	5705.	5705.	164.	147.	17.	0.	100.0	89.7

1981.	7872.	7872.	184.	168.	15.	0.	100.0	91.7
1982.	5544.	5544.	150.	137.	13.	0.	100.0	91.5
1983.	7309.	7308.	191.	170.	21.	0.	100.0	89.1
1984.	5890.	5890.	148.	131.	17.	0.	100.0	88.7
1985.	5140.	5140.	145.	131.	14.	0.	100.0	90.2
1986.	7489.	7489.	199.	181.	17.	0.	100.0	91.3
1987.	7743.	7728.	199.	179.	20.	0.	99.8	89.7
1988.	6197.	6197.	167.	152.	16.	0.	100.0	90.7
1989.	6820.	6820.	162.	149.	13.	0.	100.0	91.8
1990.	7730.	7730.	204.	187.	17.	0.	100.0	91.5
1991.	7243.	7243.	192.	174.	18.	0.	100.0	90.7
1992.	9209.	9209.	223.	196.	27.	0.	100.0	88.1
1993.	6272.	6272.	188.	174.	14.	0.	100.0	92.5
1994.	6721.	6705.	155.	132.	23.	0.	99.8	84.8
1995.	7783.	7783.	185.	161.	24.	0.	100.0	87.1
1998.	2033.	2033.	71.	63.	8.	0.	100.0	88.3
1999.	4954.	4954.	143.	128.	15.	0.	100.0	89.8
2000.	5684.	5684.	124.	105.	19.	0.	100.0	84.4
2001.	4512.	4512.	117.	110.	7.	0.	100.0	94.1
2002.	4712.	4712.	136.	124.	12.	0.	100.0	91.1
2003.	5360.	5360.	140.	125.	16.	0.	100.0	88.7
2004.	6414.	6414.	144.	128.	16.	0.	100.0	88.8
2005.	4642.	4623.	110.	92.	17.	0.	99.6	84.2

HD 4 Year	Flow Vol (m3)	Flow Treated (m3)	TSS In (kg)	TSS Rem (kg)	TSS Out (kg)	TSS Byp (kg)	Flow Treated (%)	TSS Removal (%)
1971.	4210.	4195.	102.	91.	10.	0.	99.7	90.0
1972.	5414.	5025.	134.	125.	8.	4.	92.8	91.0
1973.	5371.	5371.	144.	135.	10.	0.	100.0	93.4
1974.	5486.	5468.	154.	148.	7.	0.	99.7	95.5
1975.	4647.	4647.	132.	122.	10.	0.	100.0	92.1
1976.	6916.	6849.	165.	156.	10.	1.	99.0	93.6
1977.	7413.	7320.	161.	145.	16.	1.	98.7	89.1
1978.	5913.	5913.	153.	140.	13.	0.	100.0	91.2
1979.	7080.	7031.	176.	163.	13.	0.	99.3	92.5
1980.	5705.	5705.	164.	152.	12.	0.	100.0	92.5
1981.	7872.	7872.	184.	175.	9.	0.	100.0	95.2
1982.	5544.	5544.	150.	143.	6.	0.	100.0	95.8
1983.	7309.	7308.	191.	178.	13.	0.	100.0	92.9
1984.	5890.	5890.	148.	137.	11.	0.	100.0	92.6
1985.	5140.	5140.	145.	137.	9.	0.	100.0	94.1
1986.	7489.	7489.	199.	188.	11.	0.	100.0	94.6
1987.	7743.	7728.	199.	186.	13.	0.	99.8	93.4
1988.	6197.	6197.	167.	158.	9.	0.	100.0	94.7
1989.	6820.	6820.	162.	154.	8.	0.	100.0	95.2
1990.	7730.	7730.	204.	195.	9.	0.	100.0	95.4
1991.	7243.	7243.	192.	180.	12.	0.	100.0	93.9
1992.	9209.	9209.	223.	206.	16.	0.	100.0	92.6
1993.	6272.	6272.	188.	179.	9.	0.	100.0	95.1
1994.	6721.	6705.	155.	141.	14.	0.	99.8	90.6
1995.	7783.	7783.	185.	170.	15.	0.	100.0	91.8
1998.	2033.	2033.	71.	66.	5.	0.	100.0	92.8
1999.	4954.	4954.	143.	133.	10.	0.	100.0	93.2
2000.	5684.	5684.	124.	110.	14.	0.	100.0	89.0
2001.	4512.	4512.	117.	112.	4.	0.	100.0	96.3
2002.	4712.	4712.	136.	129.	7.	0.	100.0	94.8
2003.	5360.	5360.	140.	129.	12.	0.	100.0	91.8
2004.	6414.	6414.	144.	134.	10.	0.	100.0	93.3
2005.	4642.	4623.	110.	97.	13.	0.	99.6	88.0

 * Summary of Quantity and Quality Results at *
 * Location 200 INFlow in cms. *
 * Values are instantaneous at indicated time step *

Date Mo/Da/Year	Time Hr:Min	Flow cum/s	Total Su mg/l
-----	-----	-----	-----
Flow wtd means....		0.000	128.
Flow wtd std devs..		0.001	66.
Maximum value.....		0.158	292.
Minimum value.....		0.000	0.
Total loads.....		40281.	5169.
		Cub-Met	KILOGRAM

==> Runoff simulation ended normally.

==> SWMM 4.4 simulation ended normally.
 Always check output file for possible warning messages.

 * SWMM 4.4 Simulation Date and Time Summary *

 * Starting Date... April 5, 2023 *
 * Time... 14:57:12.691 *
 * Ending Date... April 5, 2023 *
 * Time... 14:57:16.237 *
 * Elapsed Time... 0.059 minutes. *
 * Elapsed Time... 3.546 seconds. *
