



STORMWATER MANAGEMENT REPORT

Times Group Corp.

Type of Document:

Final Report

Project Name:

1544 & 1546 Four Mile Creek Road, Niagara on the Lake

Project Number:

ALL-24011473-A0

Prepared and Reviewed By:

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Approved By:

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Date + Time Submitted:

2025-04-21

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1. Introduction

EXP Services Inc. has been retained by Times Group Corp. ("Owner") to prepare a Stormwater Management (SWM) Report ("report") in support of an application (ZBA) requesting the removal of the Holding Provision for the redevelopment of the site located at 1544 & 1546 Four Mile Creek Road, ("site") in the Town of Niagara-on-the-Lake.

The subject site is approximately 1.07 ha in area and is located on the west side of Four Mile Creek Road, just north of the Line 2 Road and Four Mile Creek Road intersection. The site is currently occupied with a residential home and commercial garage with driveway access to Four Mile Creek Road. The site is bound by Four Mile Creek Road to the east, existing residential homes to the south, woodlot lands and reservoir (Lower Virgil Reservoir) to the west and north. Finally, due to various hazards associated with the woodlot and reservoir lands to the west a small portion of the site is regulated by the Niagara Peninsula Conservation Authority (NPCA). Refer to Figure 1 for the Location Plan.

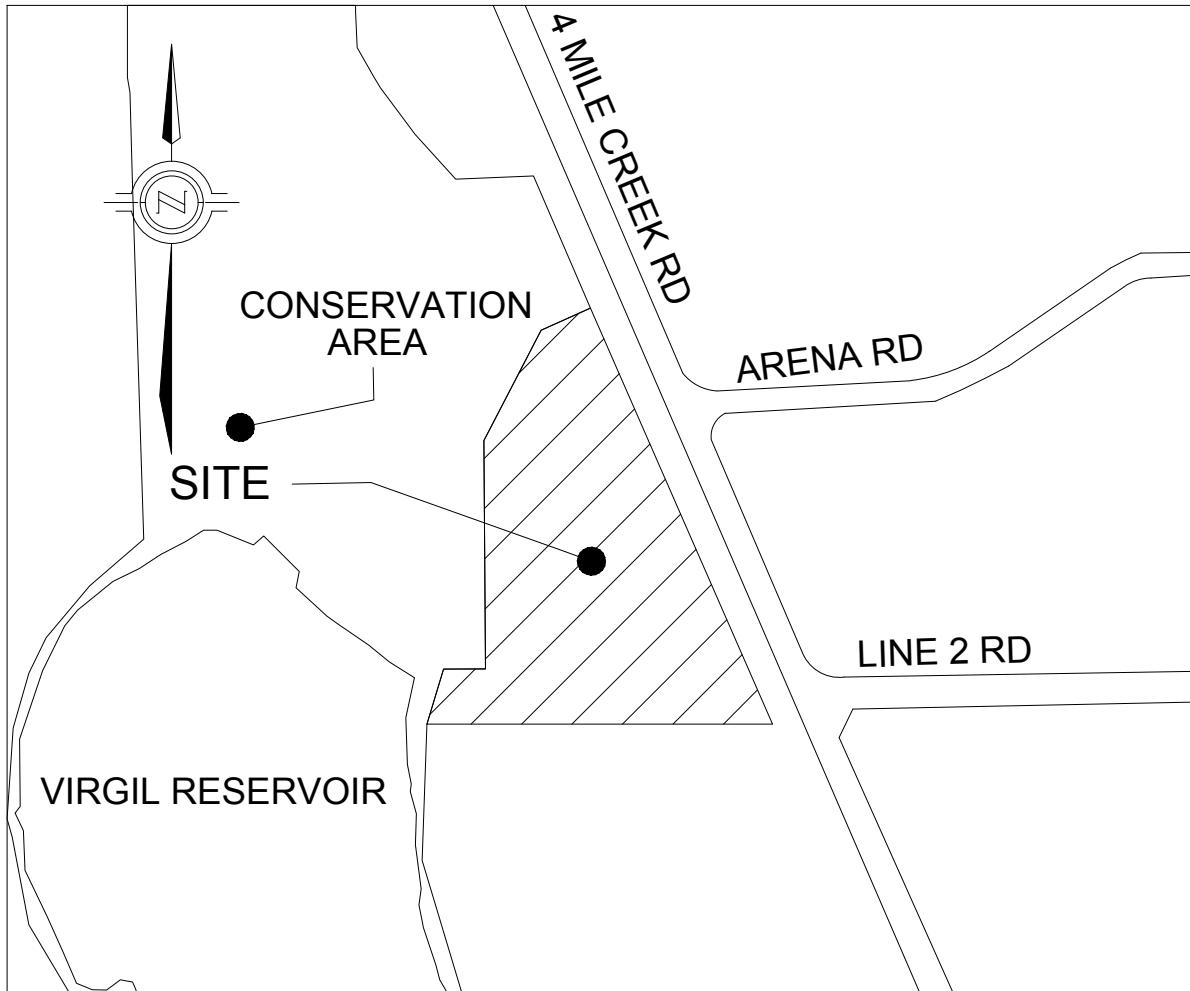
This report is intended to provide the proposed SWM strategy for the site while demonstrating conformance to Town of Niagara-on-the-Lake standards and no negative impact to neighbouring properties from the proposed development.

2. Proposed Development

The proposed redevelopment of site includes mixed commercial and residential use with two (2) separate buildings as follows:

- One (1) 2-storey commercial building of 3,699 m² GFA on the east side of the site;
- One (1) 4-storey residential building of 3,718 m² GFA and 29 units on the west side of the site;
- An underground parking structure with an envelope of approx. 4,200 m²;
- Two (2) driveway access locations to Four Mile Creek Road; and,
- Various above ground parking and landscaping across the site including boulevard improvements along Four Mile Creek Road.

Each building is to be designed with separate servicing allowances and easements for separate ownership of each building. Finally, at the southwest corner of the site there is an existing irrigation pump house connected to the Lower Virgil Reservoir where an existing irrigation line spans the south side of the site across to Four Mile Creek Road which is to be maintained. For additional details refer to the Site Plan prepared by the Icke Brochu Architects Inc in Appendix A.



E:\MRK\ALL-24011473-A0\60 Executions\65 Drawings\Civil\24011473-FIG-01 LOCATION PLAN.dwg



Project: 1544 & 1546 FOUR MILE CREEK RD, NIAGARA-ON-THE-LAKE, ON

Title: LOCATION PLAN

Approved by: S.P Date: FEB, 2025 Project No.: ALL-24011473-A0

Drawn by: R.N Scale: N.T.S. Figure no.: FIG-01

3. Existing Topography and Drainage Conditions

3.1 Site Topography

To assess the existing site topography within and surrounding the site, EXP staff reviewed topographic survey information and Town record drawings for the surrounding municipal roads. A site visit was then completed by EXP staff on February 14th, 2025 to further review existing conditions. After the review, some of the key characteristics of the existing topography can be summarized as follows.

- The majority of the site shows existing elevations generally falling in the westerly and northwesterly direction where grades fall in the approx range of 1 to 3 m;
- Along the west side of the site there is an existing steep slope with a grade change in the range of 2 m;
- A small portion of the site shows existing elevations falling in the easterly direction towards Four Mile Creek Road with shallow slopes; and,
- There is very minimal to no external drainage is observed to be conveyed across the site.

As previously mentioned, a small portion of the west side of the site is regulated by the NPCA for various hazards including floodplain and erosion setback requirements. EXP staff contacted the NPCA to obtain the most current floodplain mapping and flood elevations and transposed the elevations against the actual topographic survey completed for the site. The floodplain mapping review showed that all flood elevations (and 7.5 m development setbacks) were clear of the proposed building locations. Finally, as part of the various studies prepared by the Owner, a slope stability study was completed by EXP to ensure the appropriate setbacks are maintained. For NPCA background information refer to Appendix A.

3.2 Existing Municipal Storm Sewers

Available record drawings showing the following existing municipal storm sewers and drainage features surrounding the site:

- 525 to 1050 mm diameter storm sewers located on the west side of Four Mile Creek Road flowing in the northerly direction;
- Various roadside ditches and culverts under driveways within the Four Mile Creek Road right of way conveying flows in the northerly direction; and,
- An existing storm sewer concrete headwall outlet located within the NPCA lands adjacent to the north side of the site discharging the flows from the municipal storm sewer system on Four Mile Creek Road.

Based on the review of the available records, it is believed that there aren't any existing storm sewer service connections to the existing storm sewer on Four Mile Creek Road for each of the properties within the site. The Town's record drawings showing the storm sewer information can be found in Appendix A for reference.

3.3 Existing Conditions Peak Flows

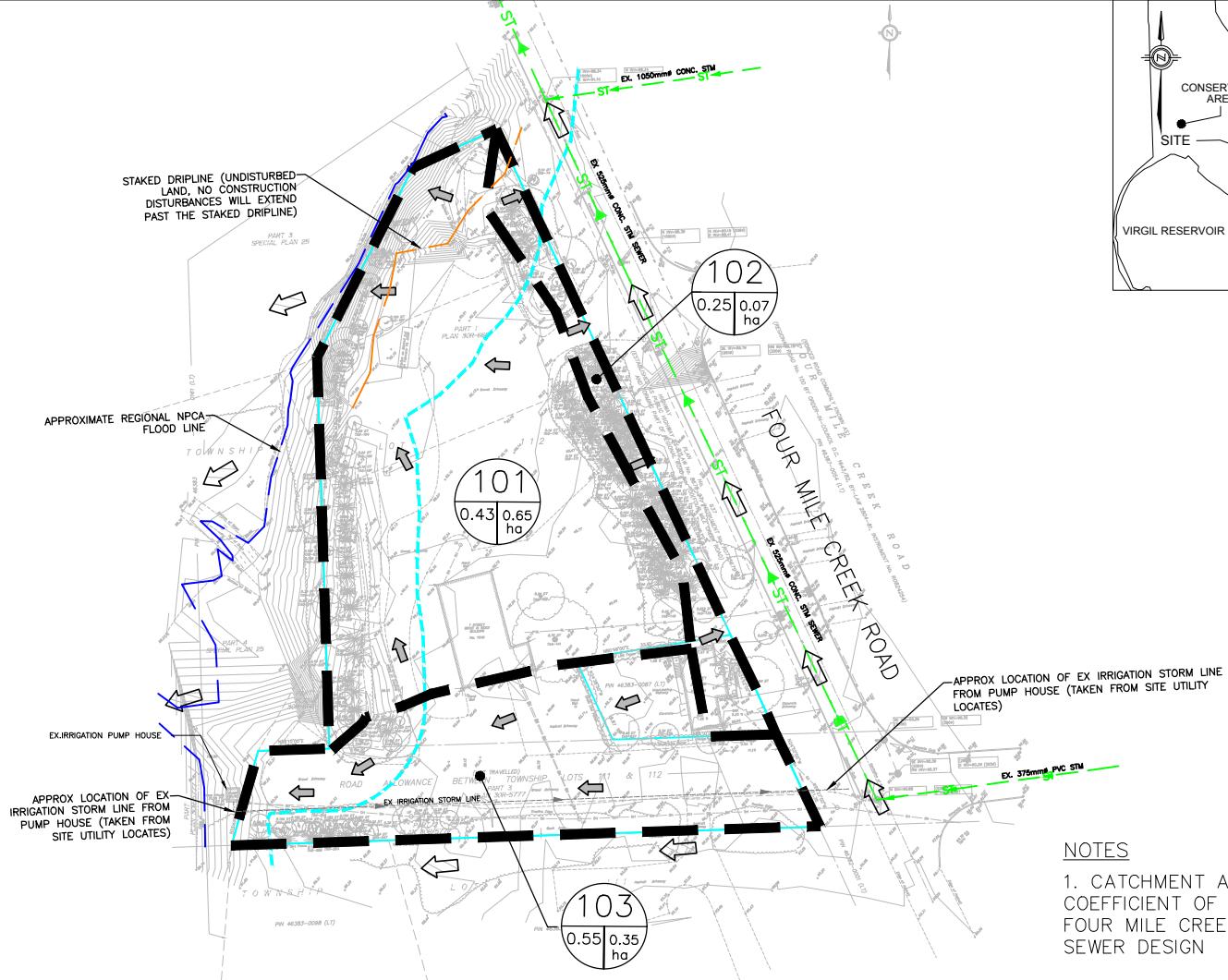
To simulate the existing drainage conditions, EXP staff calculated the peak flows using the design parameters outlined within the Town of Niagara-on-the-Lake standards and the modified Rational Method. The resultant peak flows for all storm events under existing conditions are summarized in Table 1 below:

Table 1: Peak Flow Summary (Existing Conditions)

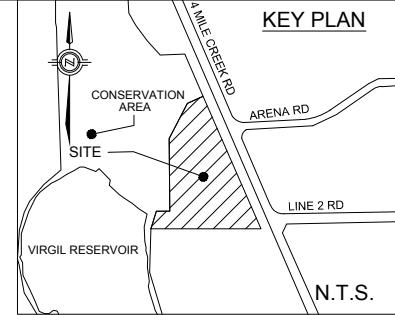
| Outlet Location | Catchment Area ID# | Area (ha) | Runoff Coefficient | Peak Flow (L/sec) | |
|---------------------------------------|--------------------|-------------|--------------------|-------------------|--------------|
| | | | | 5-Year | 100-Year |
| Four Mile Creek Road (East)* | 102 | 0.07 | 0.25 | 4.4 | 7.0 |
| | Sub-Total = | 0.07 | 0.25 | 4.4 | 7.0 |
| | 101 | 0.65 | 0.43 | 69.8 | 112.0 |
| NPCA Conservation Lands (West) | 103 | 0.35 | 0.55 | 48.1 | 77.1 |
| | Sub-Total = | 1.00 | 0.47 | 117.9 | 189.1 |
| | Total= | 1.07 | 0.45 | 122.3 | 196.1 |

*Note: It is estimated that a minimum allowance of 0.4 ha @ C=0.65 was provided in the Four Mile Creek Road municipal storm sewer design as allocation for the site (see next section in SWM report for details) for the 5-year storm = 64.9 L/s

As previously mentioned, based on the existing topography and the high point drainage divide along the east side of the site, the majority of the site drains in the westerly direction to the NPCA Conservation Lands located to the west of the property. EXP staff then reviewed available record drawings for the existing municipal storm sewer along Four Mile Creek Road to review the possible design allowances within the previous storm sewer design. After the review, it was confirmed that a previous allocation of 0.40 ha (at C=0.65) should have been maintained for the site and should be referenced when considering allowable release rates prior to discharging to the existing municipal storm sewer. The details of the proposed servicing design and SWM control release rates are discussed further in the next section. For details regarding the Existing Drainage Conditions Plan refer to Figure 2. The Peak flow runoff calculations can be found in Appendix B.



KEY PLAN



NOTES

1. CATCHMENT AREA OF 0.4 ha @ COEFFICIENT OF 0.65 ASSUMED WITHIN FOUR MILE CREEK MUNICIPAL STORM SEWER DESIGN

LEGEND

| |
|--------------------------------|
| PROPERTY LINE |
| EXISTING STORM SYSTEM |
| EXISTING GRADE |
| OVERLAND FLOW DIRECTION |
| EXTERNAL FLOW DIRECTION |
| STORM DRAINAGE ID NUMBER |
| AREA (ha) |
| RUNOFF COEFFICIENT |
| APPROX. NPCA REGULATED LIMITS |
| EXISTING STORM IRRIGATION LINE |
| CATCHMENT BOUNDARY |

Project:

1544 & 1546 FOUR MILE CREEK ROAD,
NIAGARA-ON-THE-LAKE, ONTARIO

Title:

EXISTING CONDITIONS DRAINAGE PLAN

Approved by:

S.P

Date:

APR, 2025

Project No.:

ALL-24011473-A0

Drawn by:

R.N

Scale:

1:1500

Figure no.:

FIG-02

exp.

4. Proposed Drainage Conditions

4.1 Proposed Grading

The proposed preliminary grading design for the site was completed in concert with the proposed stormwater management strategy for the site which included various pre-consultations with the owner. Some of the key features of the preliminary grading design can be summarized as follows:

- Meeting all existing elevations along the south, west and north property lines adjacent to the site;
- Modifying existing elevations along the east side of the site adjacent to the Four Mile Creek Road right of way to ensure positive drainage as part of boulevard improvement works;
- Maintaining maintenance access to the existing Lower Virgil Reservoir gates and irrigation pumphouse located at the southwest corner of the site;
- Incorporating a network of high and low points with various inlets designed to capture and convey the 100-year storm event; and,
- Grading such that major overland flow is directed away from the buildings to the Four Mile Creek Road right of way or NPCA lands in accordance to allowable release rates ensuring positive drainage across the site.

For additional grading details refer to the Preliminary Grading Plan Drawing SG-1 provided in Appendix A.

4.2 Background Information and Methodology

Some of the key documents that were referenced for completing the SWM design for the site can be summarized as follows:

- Township of Niagara-on-the-Lake Municipal Engineering Standards, dated November 2020;
- Niagara Region Water and Wastewater Master Servicing Plan 2021;
- Development Charges Background Study dated May 2022;
- Niagara Region Stormwater Management Guidelines dated December 2022;
- Niagara Peninsula Conservation Authority (NPCA) Stormwater Management Guidelines (2022);
- Niagara Peninsula Conservation Authority (NPCA) Flood Plain Mapping; and,
- Ministry of Environment, Conservation and Parks - Stormwater Management Planning and Design Manual (2003).

For any detailed peak flow runoff calculations, the Modified Rational Method was used.

4.3 Proposed Conditions Peak Flows

Based on the proposed grading and servicing design for the site, the drainage areas were reviewed to assess the runoff coefficients for each catchment. The proposed drainage from the site was then generally divided into two (2) main catchments where the corresponding drainage areas and runoff coefficients are shown on the Proposed Conditions Drainage Plan on Figure 3.

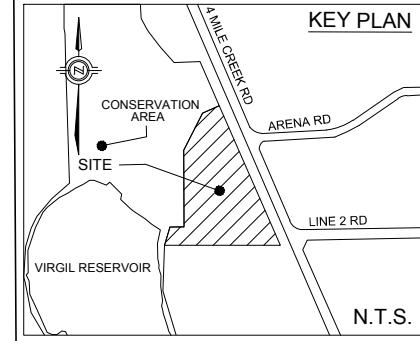
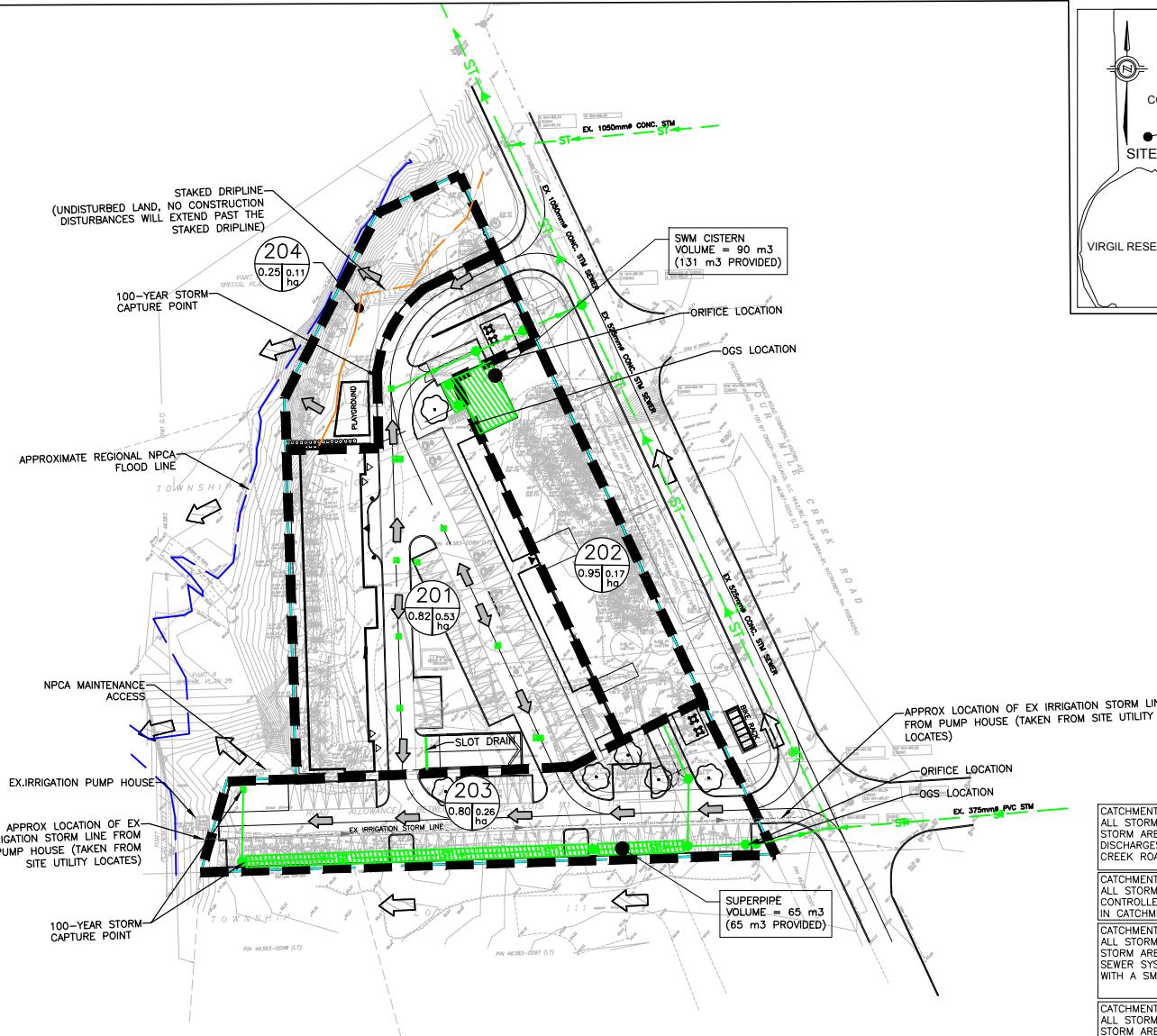
The resultant peak flows for the proposed conditions without any SWM controls and assuming 100-year storm capture are summarized in Table 2 below:

Table 2: Peak Flow Summary (Proposed Conditions– No SWM Controls)

| Outlet | Catchment ID No. | Area (ha) | Runoff Coefficient | Peak Flow (L/sec) | |
|---------------------------------------|------------------|-------------|--------------------|-------------------|--------------|
| | | | | 5-Year | 100-Year |
| Four Mile Creek Road (East) | 201 | 0.53 | 0.82 | 108.5 | 174.2 |
| | 202 | 0.17 | 0.95 | 40.3 | 64.7 |
| | 203* | 0.26 | 0.80 | 51.9* | 70.5 |
| Sub-Total = | | 0.96 | 0.80 | 200.7 | 309.4 |
| NPCA Conservation Lands (West) | 203* | N/A* | 0.80 | 0.0 | 12.8 |
| | 204 | 0.11 | 0.25 | 6.9 | 11.0 |
| Sub-Total= | | 0.11 | 0.40 | 6.9 | 23.8 |
| Total= | | 1.07 | 0.75 | 207.6 | 333.2 |

*Note: For Catchment Area #203, the 5-year flow to discharge to Four Mile Creek Road as part of the minor system and balance of major overland flow to discharge west to NPCA Conservation Lands

Therefore, resultant peak flow rates during proposed conditions showed an increase in runoff during the 100-year storm event of approximately 137.1 L/s (333.2 L/s proposed – 196.1 L/s existing). EXP staff then reviewed the requirements for the SWM quantity control for each of the two catchments which are discussed further in the next section. The Peak flow runoff calculations can be found in Appendix C.



Project:

1544 FOUR MILE CREEK ROAD, NIAGARA-ON-THE-LAKE, ONTARIO

Title:

PROPOSED CONDITIONS DRAINAGE PLAN

Approved by:

S.P

Date:

APR, 2025

Project No.:

ALL-24011473-A0

Drawn by:

R.N

Scale:

1:1500

Figure no.:

FIG-03

4.4 Proposed SWM Quantity Controls

In order to determine the required SWM quantity controls for the site, EXP staff first carefully reviewed the Niagara Region's record drawings and municipal engineering design standards. Municipal design criteria state that all post development flows must be controlled to existing conditions for all storm events up to and including the 100-year storm event. As previously mentioned, in order to provide an acceptable storm outlet for the site into the municipal storm system, EXP carefully reviewed the design allocation for the existing 525 mm diameter storm sewer along Four Mile Creek Road where it was calculated that an allocation of 0.40 ha ($C=0.65$) should be considered for the site, all pending Town approval.

Therefore, the allowable release rate for proposed storm connection from the site was calculated as follows:

North Storm Service Connection (Residential Building & U/G Parking Envelope):

To calculate the existing storm flows that tributary existing 525 mm diameter municipal sewer on Four Mile Creek Road, the following calculations were made:

| | |
|-------------------------------------|-----------|
| Site area contribution to sewer (A) | = 0.26 ha |
| Run off coefficient (C) | = 0.65 |
| Time of Concentration (Tc) | = 10 min |

Niagara Region's 5-year Intensity (I) Formula: $I = A/(T_c+B)^C$
 Where:
 I = Rainfall intensity in mm/hour
 T_c = time of concentration in hours
 $A = 664, B = 4.7 C = 0.744$

Therefore: Intensity (I) = $(664/(10+4.7))^{0.744}$
 $= 89.88 \text{ mm/hr}$

Rational Method Formula: $Q = 2.78 * C * I * A$
 Therefore: $Q = 2.78 * 0.65 * 89.88 * 0.26$
 $= \underline{\underline{42.2 \text{ L/s}}}$

South Storm Service Connection (Commercial Building & South Parking Areas):

To calculate the existing storm flows that tributary to existing 525 mm diameter municipal sewer on Four Mile Creek Road, the following calculations were made:

| | |
|---|-----------|
| Site area contribution to South sewer (A) | = 0.14 ha |
| Run off coefficient (C) | = 0.65 |
| Time of Concentration (Tc) | = 10 mins |

Niagara Region's 5-year Intensity (I) Formula: $I = A/(T_c+B)^C$
 Where:
 I = Rainfall intensity in mm/hour
 T_c = time of concentration in hours
 $A = 664, B = 4.7 C = 0.744$

Therefore: Intensity (I) = $(664 / (10 + 4.7))^0.744$
 = 89.88 mm/hr

Rational Method Formula: $Q = 2.78 * C * I * A$
 Therefore: $Q = 2.78 * 0.65 * 89.88 * 0.14$
 = 22.7 L/s

EXP staff then moved forward to develop the proposed stormwater management (SWM) quantity controls for the site which can be summarized as follows:

- Minor storm sewer systems to be designed for a maximum allowable storm release rate to existing 525 mm storm sewer on Four Mile Creek Road 42.2 L/s (North) and 22.7 L/s (South) for the site
- Any major overland flow spilling to the NPCA Conservation Lands to the west to not exceed existing conditions
- For the north system, provide an underground SWM cistern within underground parking envelope of approximately 90 m³ volume; and,
- For the south system, provide an underground Superpipe system as part of the site storm servicing design of approximately 65 m³ volume.

As previously mentioned, in order to meet the maximum allowable release rate for the site, the proposed storm servicing design incorporated the use of Two (2) orifice controls: 100 mm diameter (North), 85 mm diameter (South). The orifice controls are positioned upstream of the proposed SWM quality controls (Oil Grit Separator) prior to connecting to the existing municipal storm sewer systems at each outlet point.

The resultant peak flows under proposed with the implementation of the proposed SWM controls can be summarized in Table 3 below:

Table 3: Peak Flow Summary (Proposed Conditions – with SWM Controls)

| Outlet | Catchment ID No. | Area (ha) | Runoff Coeff | Allowable Release Rate (L/s) | Peak Flow (L/sec) To be controlled | | Storage Required (m ³) | Storage Provided (m ³) |
|-------------------------------|------------------|-------------|--------------|------------------------------|------------------------------------|--------------|------------------------------------|--------------------------------------|
| | | | | | 5-Year | 100-Year | | |
| Four Mile Creek Road (East) | 201 | 0.53 | 0.82 | 42.22 | 108.5 | 174.2 | 90 | 100 (41 L/s release rate) |
| | 202 | 0.17 | 0.95 | 22.73 | 40.3 | 64.7 | 65 | 65 (22 L/s release rate) |
| | 203** | 0.26 | 0.80 | | 43.9 | 70.5 | | |
| Sub-Total= | | 0.96 | 0.80 | 64.95 | 192.7 | 309.4 | 155 | 165 (flow rate < 64.9 L/s) |
| NPCA Conservation Area (West) | 203** | N/A** | 0.80 | 87.25 | 0.0 | 12.8 | N/A | N/A |
| | 204* | 0.11 | 0.25 | 11.00 | 6.9 | 11.0 | N/A | N/A |
| Sub-Total = | | 0.11 | 0.40 | 98.25 | 6.9 | 23.8 | N/A | N/A |
| Total= | | 1.07 | 0.74 | 163.15 | 199.6 | 333.2 | 155 | |

* Note: Area is uncontrolled without any SWM controls

**Note: For Catchment Area #203, the 5-year flow to discharge to Four Mile Creek Road as part of the minor system and balance of major overland flow to discharge west to NPCA Conservation Lands

Overall, the actual release rates of the proposed SWM quantity controls can meet the maximum allowable release rates for the site before connecting to the municipal storm system. For additional details regarding the Proposed Drainage Conditions Plan refer to Figure 3. For additional reference, the Preliminary Site Grading and Servicing Plans have been provided in Appendix A. Finally, the peak flow runoff calculations can be found in Appendix C.

4.5 Proposed SWM Quality Controls

The Town of Niagara-on-the-Lake requires the long-term average removal of 80% total suspended solids (TSS) on an annual loading basis from all runoffs leaving the proposed development site based on the post development level of imperviousness. This requirement for the long-term removal average of 80% TSS is consistent with the “Enhanced Protection” levels recommended in MECP SWM Planning and Design Manual. After review of the owner’s site development, it was determined that two (2) oil and grit separators (OGS) are required downstream of orifice controls to treat storm flows prior to being discharged to the municipal storm sewer on Four Mile Creek Road. The OGS specifications are to be finalized as part of the future detailed site SWM design during the SPA stage.

5. Erosion and Sediment Controls during Construction

During construction it is imperative that the contractor installs and maintains all the necessary erosion and sediment control (ESC) measures to ensure there is no negative impact to surrounding properties and the local municipal sewer systems.

Outside the site, sediment control measures such as catchbasin silt sacks are to be installed inside the existing catchbasins along Four Mile Creek Road immediately adjacent to the site. These silt sacks are to be monitored and maintained after all rainfall events.

Within the site, silt fencing is required to be installed around the perimeter of the site during grading and building activity to ensure sediment is not transported overland during a rainfall event to neighbouring properties and Four Mile Creek. Similar to the required silt sacks within the catchbasins along Four Mile Creek Road, the silt fence is to be monitored after every rainfall event and repaired as necessary. Mud tracking from construction truck transport is to be mitigated through the use of mud mats and any other maintenance requirements necessary by the contractor before driving back on existing municipal roads.

Additional ESC measures not mentioned may be required through the development of the detailed design for the site and the permitting process through the Town of Niagara-on-the-Lake and the NPCA.

6. Conclusions

In summary, based on the findings in this report the proposed SWM strategy can meet the requirements of the Town and NPCA standards, where the results can be summarized as follows:

- Based on the completed topographic survey, the majority of the existing site drainage is observed to flow overland in the westerly and northwesterly directions to the existing woodlot and reservoir lands along the west side of the site as part of the Four Mile Creek watershed
- Based on the NPCA regulated mapping, a small portion of the site is regulated for various hazards including floodplain along the west side of the site due to Four Mile Creek
- Based on the Town's record drawings, there is an existing 525 mm dia storm sewer on Four Mile Creek Road conveying flows in the northerly direction to an outlet discharging to Four Mile Creek located immediately north of the site, where it is believed a pre-existing site allocation to the storm sewer of 0.40 ha ($C=0.65$) can be considered pending Town approval
- Storm servicing can be provided with the two (2) proposed storm service connections to the existing 525 mm diameter municipal storm sewer on Four Mile Creek Road
- SWM quantity controls can be provided by a proposed underground SWM cistern located within the underground parking envelope and underground superpipe located along the south side of the site, all releasing flows to the allowable release rates to the existing storm sewer on Four Mile Creek Road
- SWM quality controls can be provided by the use of two (2) oil and grit separators designed to meet the Town storm sewer discharge by law parameters including TSS removals
- Temporary erosion and sediment control measures during construction can be provided without any negative impact to neighbouring properties or the municipal storm sewer system
- Adequate flood protection can be provided to the proposed buildings based on the proposed preliminary grading design all in accordance with NPCA standards and MNRF technical guidelines
- Emergency overland flow (flows beyond the 100-year storm) can be safely conveyed in the westerly direction towards the woodlot and reservoir lands along the west side of the site without any negative impact to neighbouring properties

Sincerely,

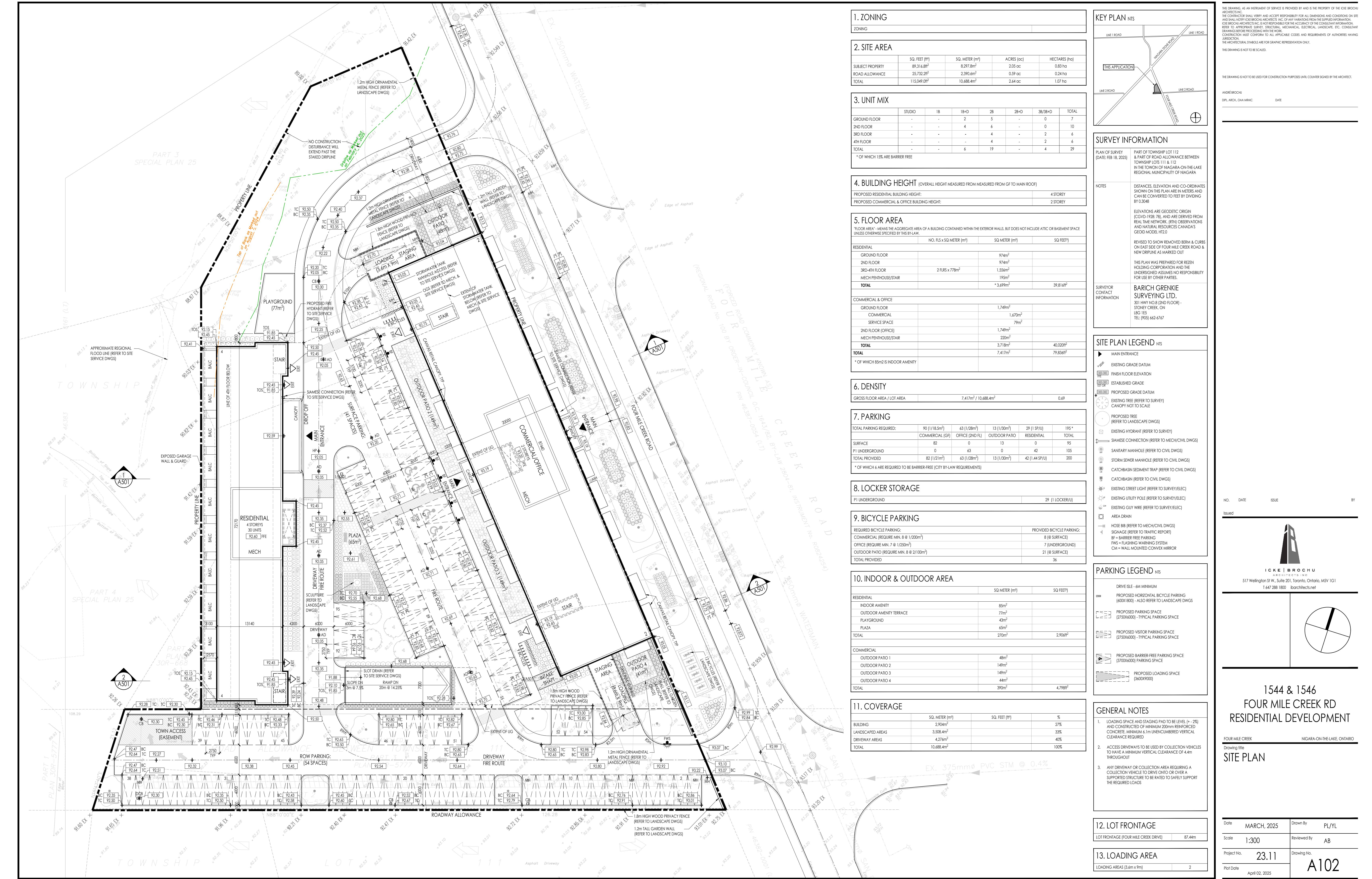
EXP Services Inc.



Scott Passmore, P.Eng.
Project Manager, Land Development

Roshawn Nunes
Project Designer, Land Development

Appendix A – Site Plan, Topographic Survey, Background Information





**PLAN OF SURVEY
(WITH TOPOGRAPHIC DETAIL) OF
PART OF TOWNSHIP LOT 112
& PART OF ROAD ALLOWANCE
BETWEEN TOWNSHIP LOTS 111 & 112
(GEOGRAPHIC TOWNSHIP OF NIAGARA)
IN THE
TOWN OF NIAGARA-ON-THE-LAKE
REGIONAL MUNICIPALITY OF NIAGARA**

SCALE: 1:500
BARICH GRENKIE SURVEYING LTD.
A DIVISION OF GEOMAPLE
© COPYRIGHT 2024

METRIC
DISTANCES, ELEVATIONS AND CO-ORDINATES SHOWN ON THIS PLAN ARE IN METRES
AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

ELEVATION NOTE
ELEVATIONS ARE GEODETIC ORIGIN (GVD-1928:78), AND ARE DERIVED FROM
REAL TIME NETWORK (RTN) OBSERVATIONS AND NATURAL RESOURCES
CANADA'S GEOID MODEL HT2.0

THIS PLAN WAS PREPARED FOR REZEN HOLDING CORPORATION AND THE
UNDERSIGNED ASSUMES NO RESPONSIBILITY FOR USE BY OTHER PARTIES.

BEARING NOTE
BEARINGS ARE UTM GRID, DERIVED FROM GPS OBSERVED REFERENCE POINTS
A AND B, BY REAL TIME NETWORK (RTN) OBSERVATIONS, UTM ZONE 17 (81°
00' WEST LONGITUDE) NAD83 (CRS) (2010.0).

HORIZONTAL DATUM NOTE
PROJECTION: UNIVERSAL TRANSVERSE MERCATOR
(UTM, ZONE 17, 81° 00' W)

DATUM: NAD83 (CRS)(2010.0)

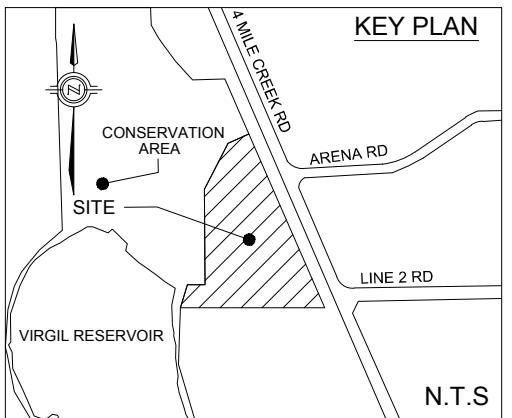
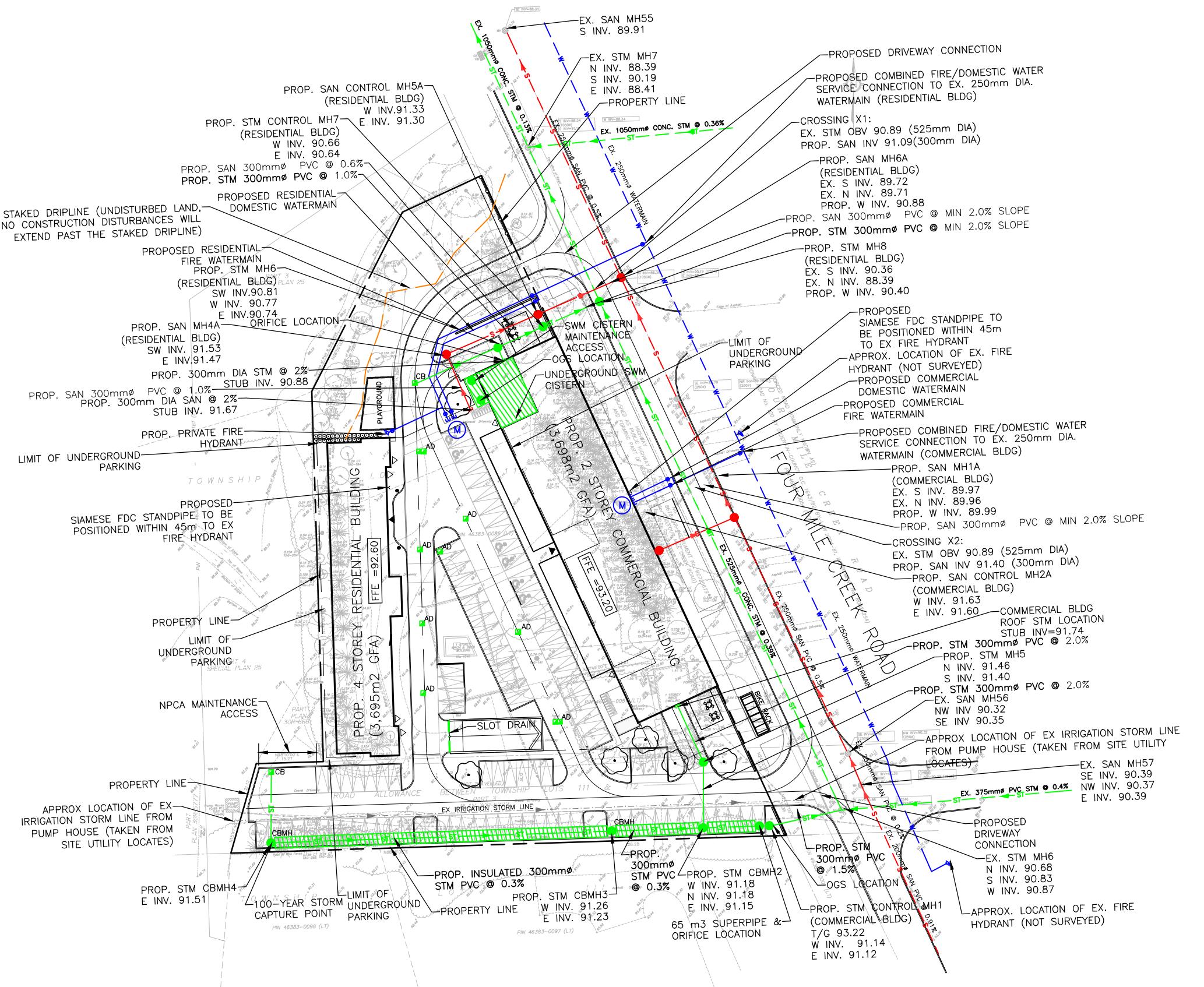
GRID SCALE CONVERSION
DISTANCES ARE GROUND AND CAN BE CONVERTED TO GRID DISTANCES BY
MULTIPLYING BY THE COMBINED SCALE FACTOR OF 0.999872.

| OBSERVED REFERENCE POINTS (ORPs) DERIVED FROM GPS OBSERVATIONS USING REAL TIME NETWORK (RTN) OBSERVATIONS UTM ZONE 17, NAD83 (CRS)(2010.0). COORDINATES TO URBAN ACCURACY PER SEC 14(2) OF OREG. 216/10 | | |
|--|-------------|------------|
| OBSERVED REFERENCE POINTS | | |
| MONUMENT ID | NORTHING | EASTING |
| A IB | 4786944.166 | 652484.398 |
| B IB | 4786733.649 | 652592.005 |

COORDINATES CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN.

| | |
|------|--------------------------------------|
| ■ | DENOTES SURVEY MONUMENT FOUND |
| □ | DENOTES SURVEY MONUMENT PLANTED |
| IB | DENOTES IRON BAR |
| SIB | DENOTES STANDARD IRON BAR |
| SSIB | DENOTES SHORT STANDARD IRON BAR |
| OU | DENOTES ORIGIN UNKNOWN |
| 539 | DENOTES D. G. URE, O.L.S. |
| 567 | DENOTES R. B. ERWIN, O.L.S. |
| 744 | DENOTES R. J. McNAUL, O.L.S. |
| 1497 | DENOTES J. P. BOUWENS, O.L.S. |
| JDB | DENOTES J. D. BARNES, O.L.S. |
| P1 | DENOTES PLAN BY J. D. BARNES LTD. |
| P2 | DENOTES DATED JULY 19, 2022 |
| MH | DENOTES SPECIAL PLAN 85 |
| CB | DENOTES MANHOLE |
| LS | DENOTES CATCHBASIN |
| TC | DENOTES LINE OF STANDARD |
| GUT | DENOTES TOP OF CURB ELEVATION |
| OH | DENOTES GUTTER ELEVATION |
| DT | DENOTES OVERHEAD UTILITY CABLES |
| CT | DENOTES DECIDUOUS TREE |
| UP | DENOTES CONIFEROUS TREE |
| PF | DENOTES UTM POST |
| FF | DENOTES FINISHED FLOOR ELEVATION |
| GF | DENOTES GARAGE FLOOR ELEVATION |
| CLF | DENOTES CHAIN LINK FENCE |
| PWF | DENOTES POST & WIRE FENCE |
| RPWF | DENOTES REMAINS OF POST & WIRE FENCE |
| GL | DENOTES GASLINE |
| BRK | DENOTES TOP NUT OF FIRE HYDRANT |
| TINH | DENOTES CONCRETE RETAINING WALL |
| CRW | |

| |
|--|
| REVISED NOTE REVISED TO SHOW REMOVED BERM & CURBS ON EAST SIDE OF FOUR MILE CREEK ROAD & NEW DRIPLINE AS MARKED OUT |
| FEBRUARY 19, 2025 |
| ERIC G. SALZER O.L.S., O.L.I.P. |
| SURVEYOR'S CERTIFICATE I CERTIFY THAT 1. THIS SURVEY AND PLAN ARE CORRECT AND IN ACCORDANCE WITH THE SURVEYS ACT, THE SURVEYORS ACT AND THE REGULATIONS MADE UNDER THEM. 2. THE SURVEY WAS COMPLETED ON JANUARY 25, 2024. |
| JANUARY 26, 2024 |
| ERIC G. SALZER O.L.S., O.L.I.P. |
| Barich Grenkie Surveying Ltd. 301 HWY No. 2, GALT, ON L9G 1E5 A DIVISION OF GEOMAPLE |
| DW BY: EGS |
| CHK BY: EWA |
| JOS No. 23-3200 |



| LEGEND: | |
|---------|-------------------------------------|
| | PROPERTY LINE |
| | NEW / EXISTING WATER VALVE AND BOX |
| | EXISTING HYDRANT |
| | PROPOSED ELEVATION |
| | EXISTING ELEVATION |
| | DRAINAGE ARROW / SLOPE (MAX 3:1) |
| | MAJOR INTERNAL OVERLAND FLOW |
| | MAJOR EXTERNAL OVERLAND FLOW |
| | EX. STORM/SANITARY M.H. |
| | EX. CATCH BASIN |
| | PROP. CATCHBASIN |
| | PROP. STORM M.H. |
| | PROP. SANITARY M.H. |
| | EX. STORM SEWER |
| | PROP. STORM SEWER |
| | EX. SAN SEWER |
| | PROP. SANITARY SEWER |
| | EX. WATERMAIN |
| | PROP. WATERMAIN |
| | PROP. SWM QUANTITY STORAGE FACILITY |
| | WATER METER LOCATION |
| | EXISTING IRRIGATION LINE |

NOTES

- TOPOGRAPHIC SURVEY PROVIDED BY BARCH GRENKE SURVEYING LTD. COMPLETED ON JANUARY 25, 2024.
- SITE PLAN PROVIDED BY ICKE BROCHU ARCHITECTS INC

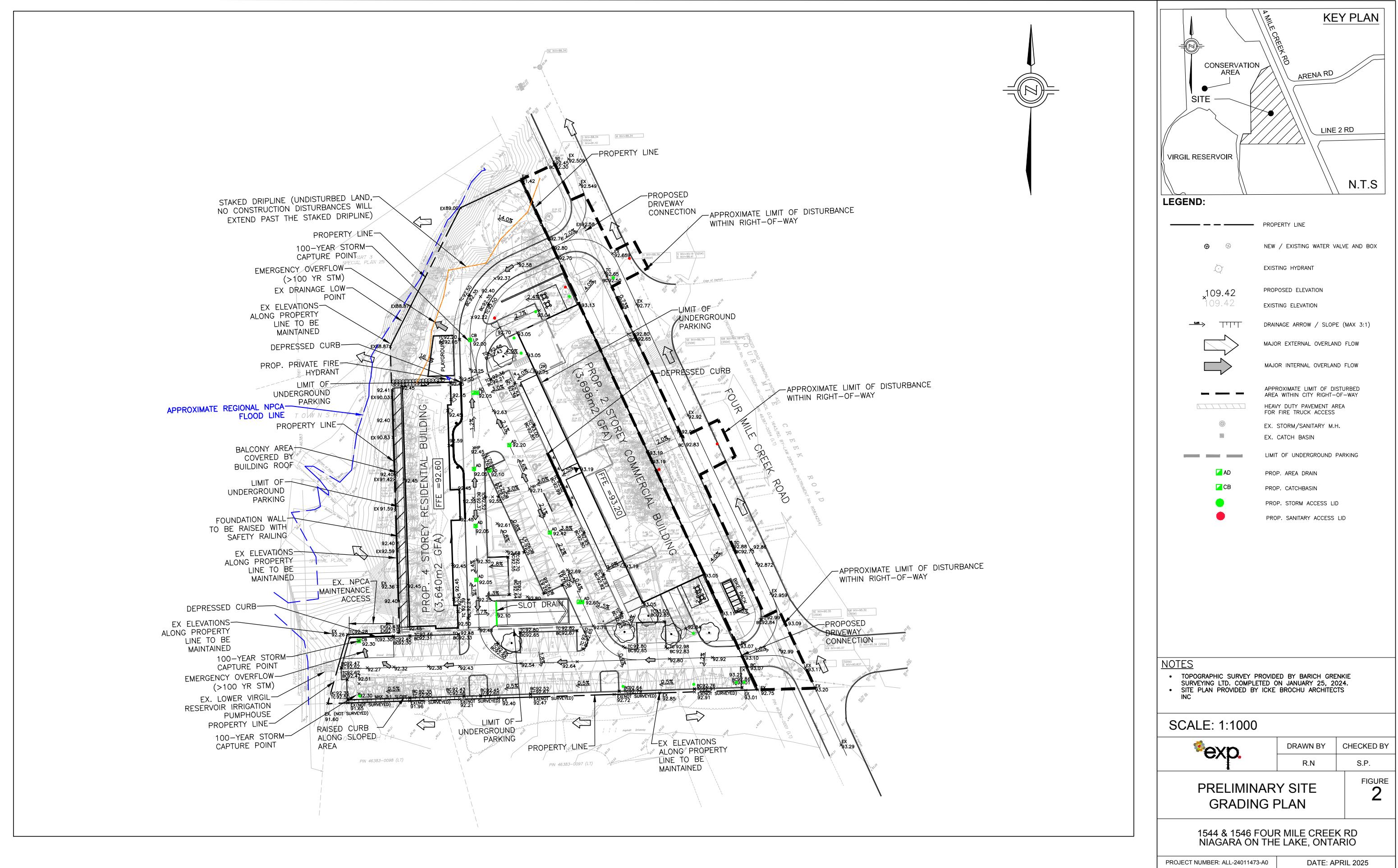
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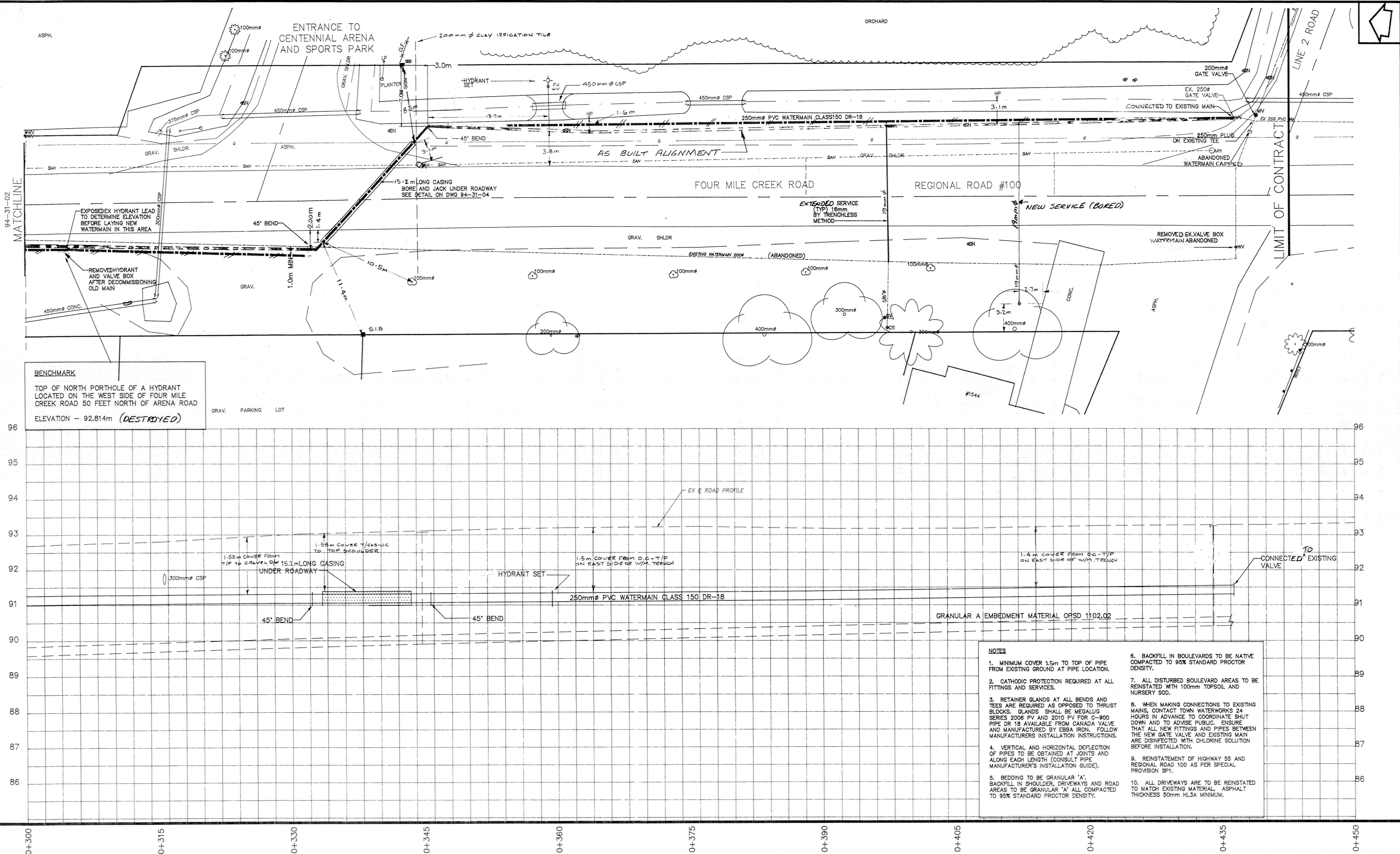
| | | |
|--|----------|------------|
| | DRAWN BY | CHECKED BY |
| | R.N | S.P. |

PRELIMINARY SITE SERVICING PLAN

FIGURE
3

1544 & 1546 FOUR MILE CREEK RD
NIAGARA ON THE LAKE, ONTARIO





GENERAL NOTE

- GENERAL NOTES:**

 - 1) THE POSITION OF POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND ABOVE-GROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND, WHERE SHOWN THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME LIABILITY FOR DAMAGE TO THEM.
 - 2) CHECK ALL DIMENSIONS AND REPORT ANY INCONSISTENCIES TO THE ENGINEER BEFORE PROCEEDING WITH THE WORK - DO NOT SCALE DRAWINGS.
 - 3) THIS DRAWING IS AN INSTRUMENT OF PROFESSIONAL SERVICE AND IS INTENDED FOR USE ONLY IN CONNECTION WITH THE PROJECT COVERED BY THE ENGINEERING AGREEMENT.

- 4) ROBERT M. MARTIN ENGINEERING & PROJECT MANAGEMENT INC. DOES NOT ASSUME ANY RESPONSIBILITY FOR LOSSES, DAMAGES AND COSTS ARISING FROM USE OR REUSE OF THIS DRAWING BY PERSONS, FIRMS OR CORPORATIONS WITHOUT PRIOR WRITTEN CONSENT OF ROBERT M. MARTIN ENGINEERING INC.
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- 6) BOREHOLE DATA SHOWN ON THE DRAWINGS IS TAKEN FROM THE GEOTECHNICAL REPORT PREPARED BY THE GEOTECHNICAL ENGINEERING CONSULTANTS. ROBERT M. MARTIN ENGINEERING INC. ASSUMES NO RESPONSIBILITY FOR THE ACCURACY OF THIS INFORMATION.

DRAFTING

AK

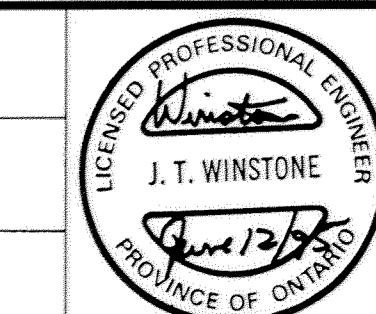
1

DESIGN

10

CHECKED

11



The logo consists of a large, bold, stylized monogram 'RM'. The 'R' has a vertical line through its center, and the 'M' has a diagonal line through its middle. To the left of the monogram is a graphic element resembling a series of vertical bars or a stylized 'E'.

Robert M. Martin Engineering
& Project Management Inc.

8 Centre Street, St. Catharines
Ontario. L2R 3A7

Phone (905) 687-4020
Fax (905) 687-4164

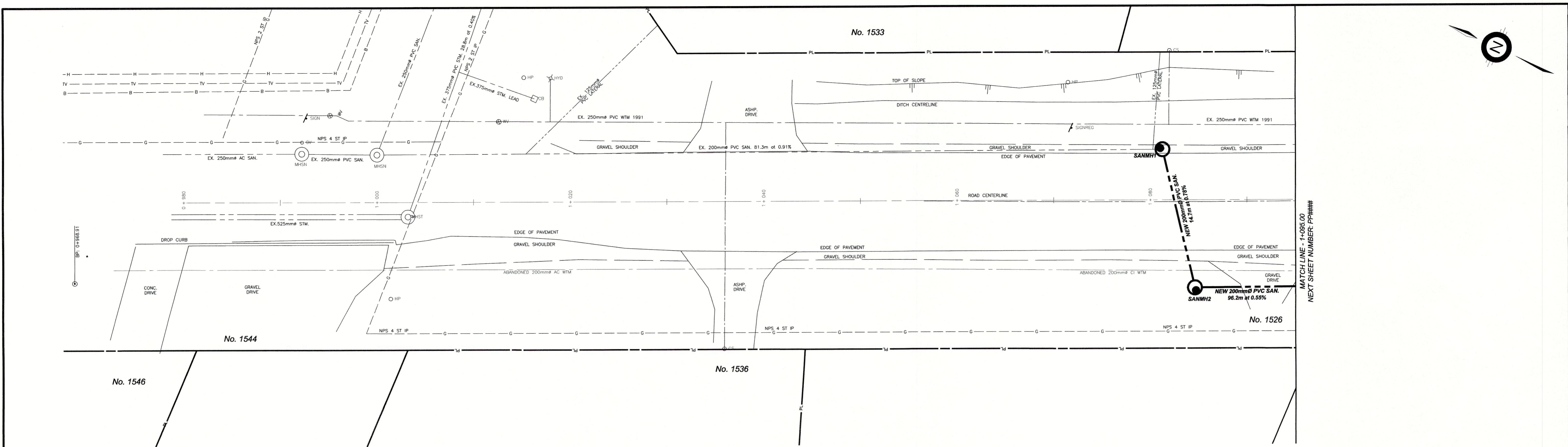
TOWN OF NIAGARA ON THE LAKE

FOUR MILE CREEK ROAD

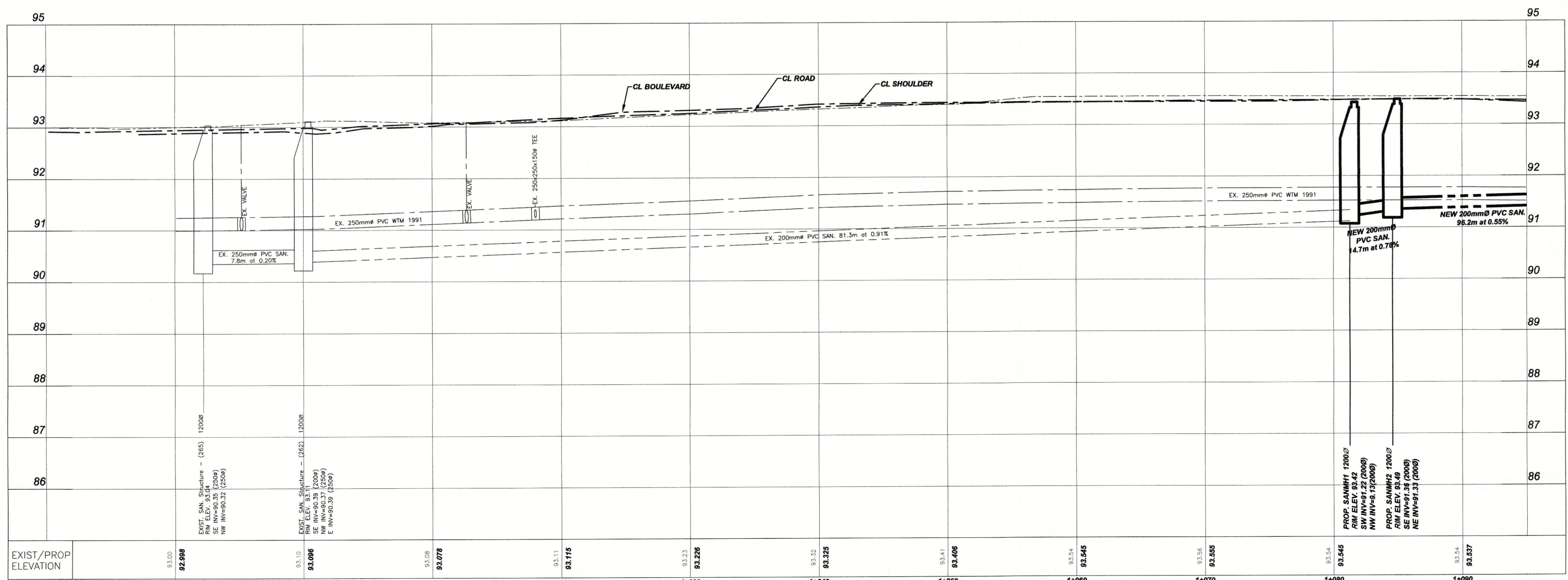
WATERMAIN REPLACEMENT

VIRGIL

| | |
|--------------|--------------|
| LENAME | 94-31\NOTL-3 |
| ATE | JUNE 1995 |
| CALE | 1:200 |
| | 1:50 |
| NG. No. | 94-31-03 |
| UN. REF. No. | REV. 1 |



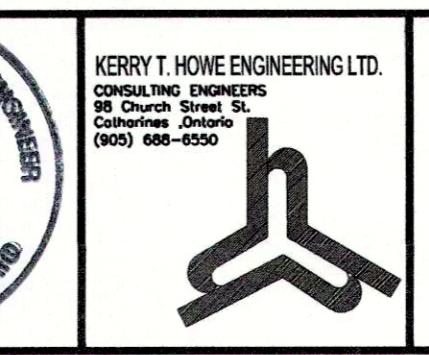
FOUR MILE CREEK ROAD (RR NO. 100)



| NOTES/LEGEND | | |
|--------------------------|----------|------|
| 6 RECORD OF CONSTRUCTION | JULY/15 | LB |
| 5 ISSUED FOR TENDER | APR/15 | LB |
| 4 REISSUED FOR MOE | MAR/15 | JH |
| 3 REISSUED FOR MOE | MAR/15 | LB |
| 2 ISSUED FOR MOE | JAN/15 | LB |
| 1 ISSUED FOR REVIEW | NOV/14 | LB |
| NO. | REVISION | DATE |
| INIT | | |

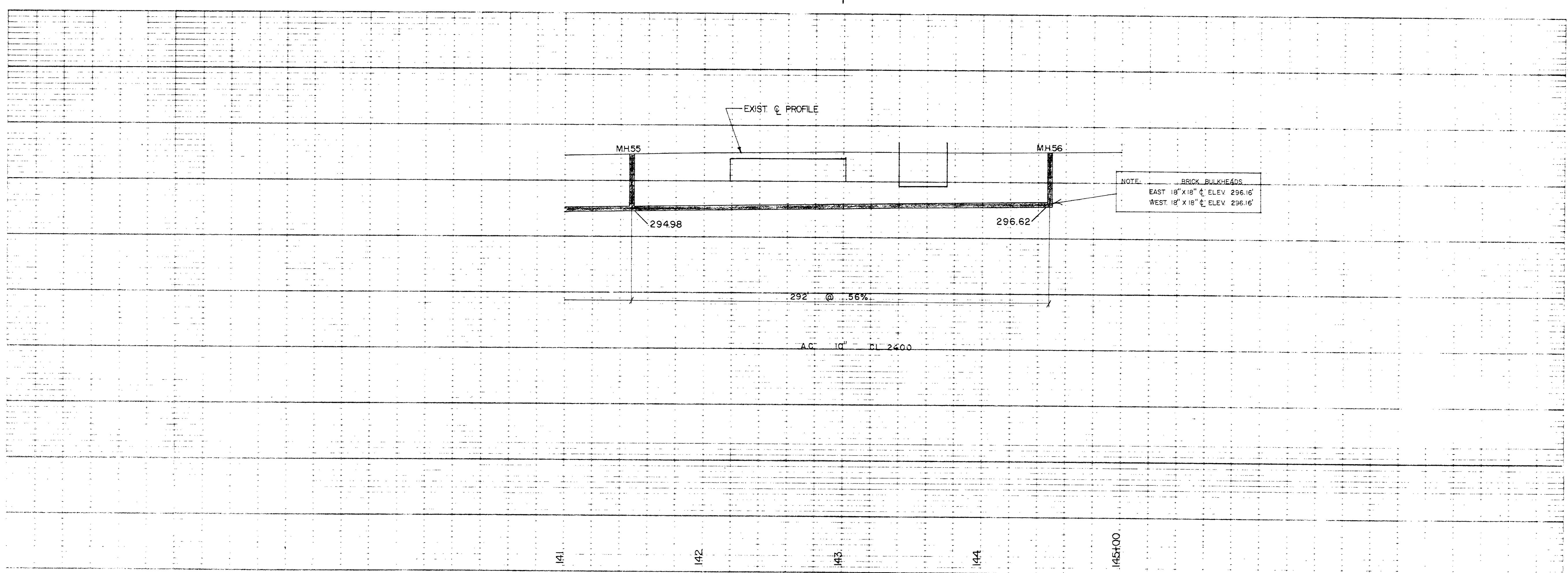
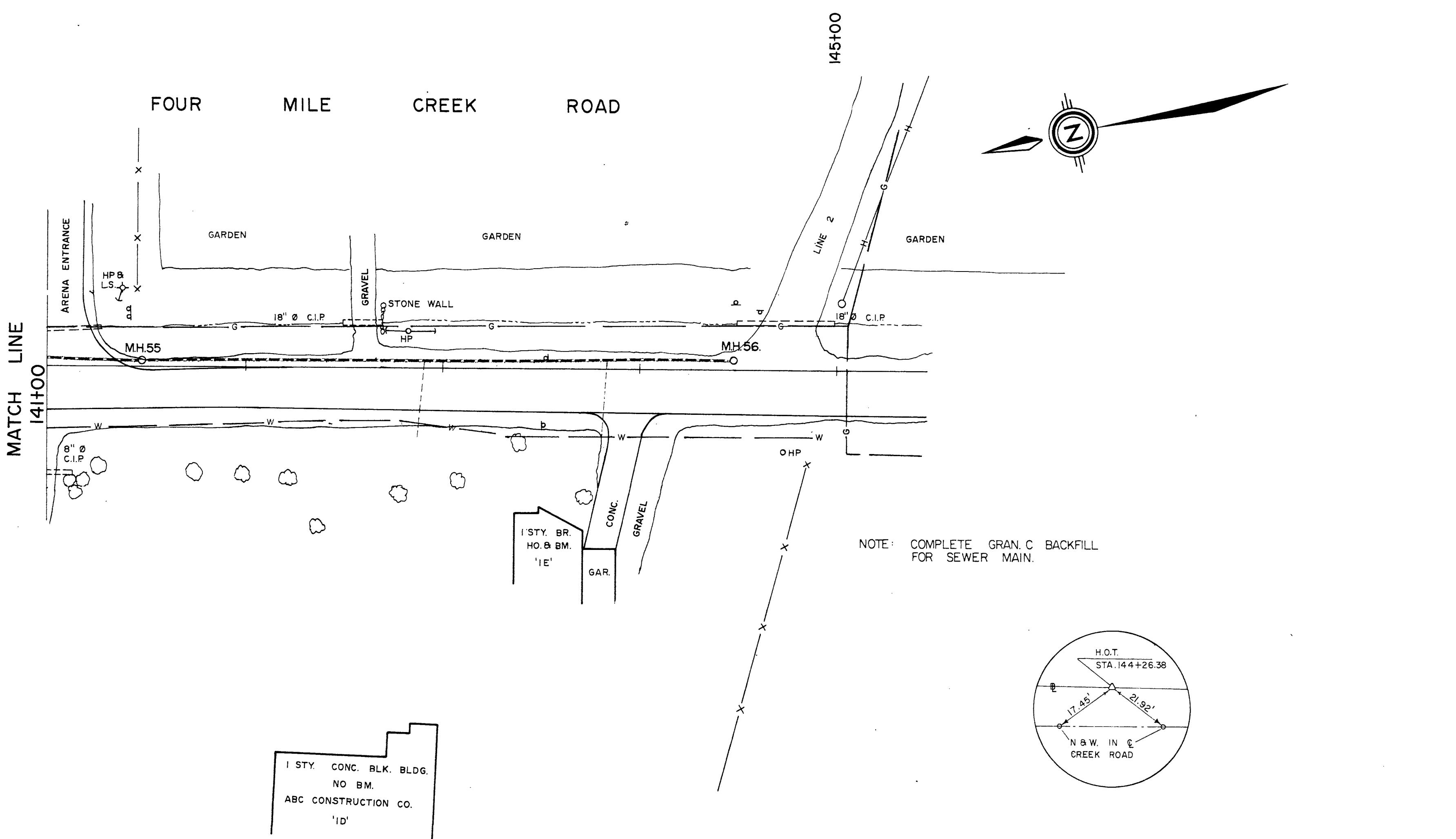
1 THE POSITION OF POLE LINES, CONDUITS, SEWER AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE COMMENCING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
 2 PROPERTY LINES WERE PLOTTED USING REGISTERED PLANS AND BARS LOCATED IN THE FIELD. TO VERIFY THE ACCURACY OF THESE PROPERTY LINES, A LEGAL BENCHMARK SHOULD BE PERFORMED PRIOR TO CONSTRUCTION.
 VERTICAL MONUMENT: ----- ELEV. -----
 DATUM: -----
 GEOGRAPHIC PROJECTION: U.T.M. NAD 83 ZONE 17

DRAFTING
LB/JH
DESIGN
KH
CHECKED BY
SK
APPROVED BY
KH



FOUR MILE CREEK ROAD (RR NO. 100)
SANITARY SEWER EXTENSION
TOWN OF NIAGARA-ON-THE-LAKE
PLAN AND PROFILE

CONSULTANT FILE No. 14-030
DATE JULY 24, 2015
SCALE HOR 1:200
VER. 1:50
REF. No. _____
DWG. No. 14-030-PP1
REV. 6



| M.H.N# | BASELINE CHAINAGE | OFFSET |
|--------|-------------------|--------|
| 55 | 141+51 | 3'S |
| 56 | 144+47 | 5'S |

| No. | REVISIONS TO DRAWING | BY | DATE | APPR. |
|--------|---------------------------|----|-------------|--------------------|
| 1 | AS CONSTRUCTED | DH | AUG, 1978 | <i>[Signature]</i> |
| | APPROVED FOR CONSTRUCTION | | Dec 8, 1978 | <i>[Signature]</i> |
| CLIENT | | | | |

MINISTRY OF THE ENVIRONMENT

MUNICIPALITY
NIAGARA-ON-THE-LAKE

PROJECT
PROVINCIAL SEWAGE WORKS PROGRAMME

SHEET TITLE
FOUR MILE CREEK ROAD
STA.141+00-STA.145+00

WILLIAM L. SEARS
AND ASSOCIATES LIMITED
CONSULTING PROFESSIONAL ENGINEERS
STONEY CREEK ONT

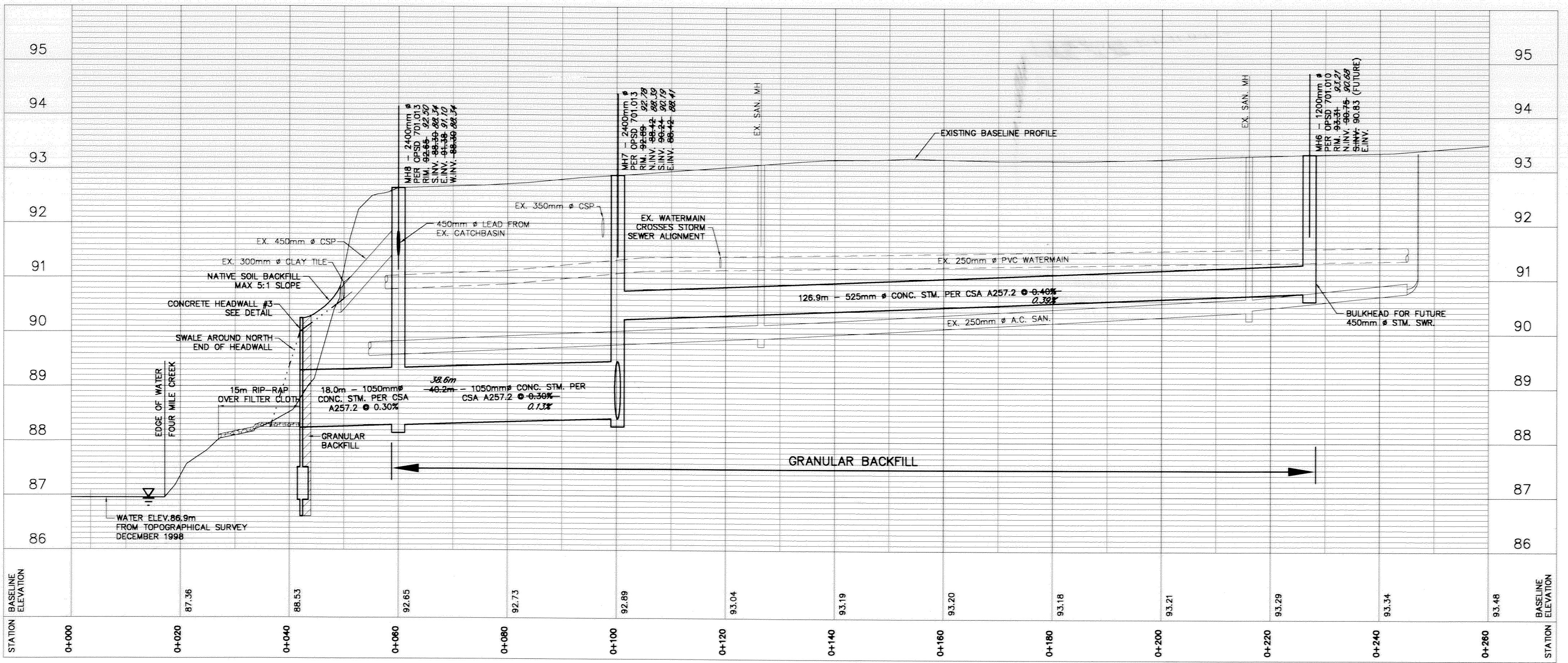
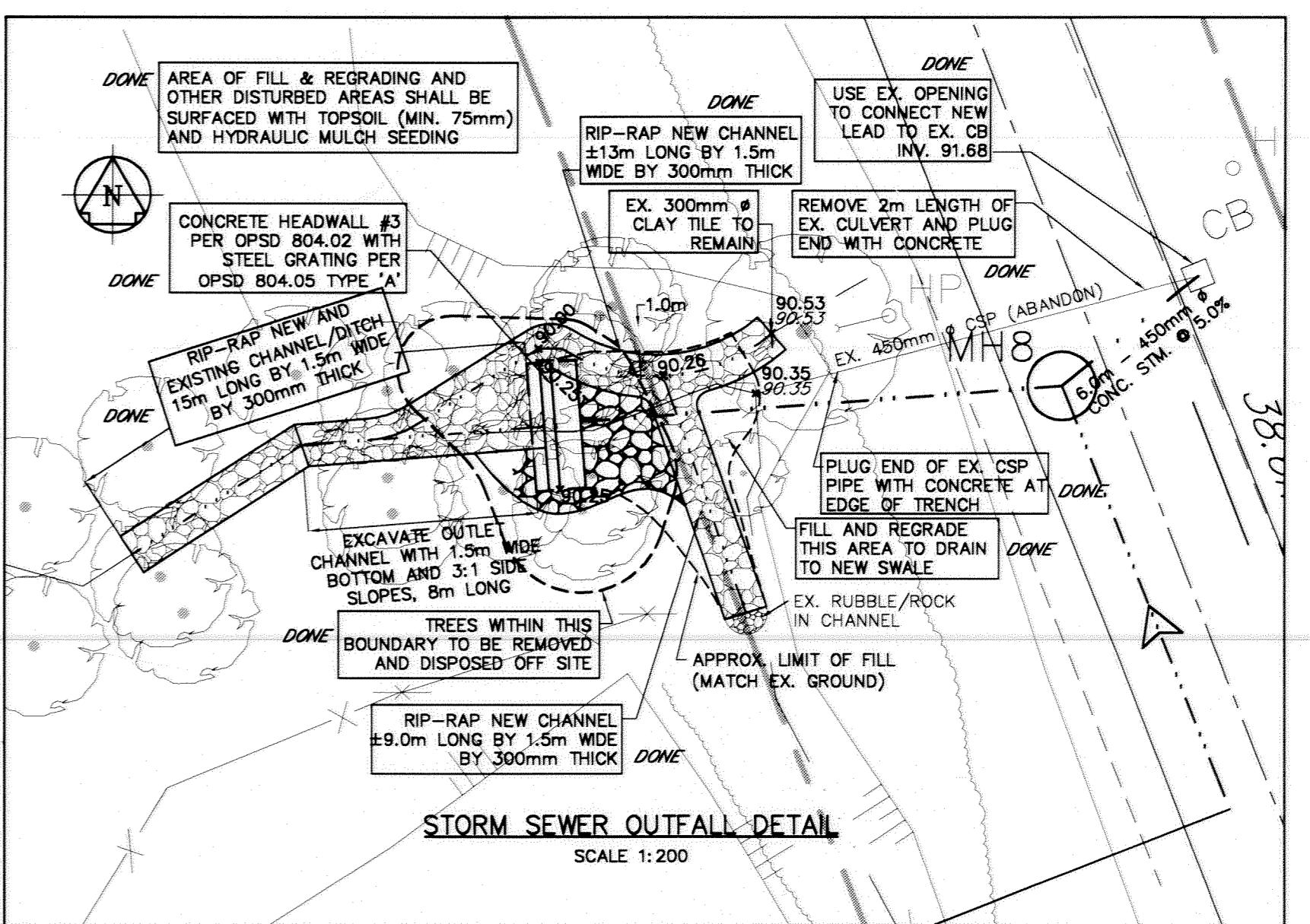
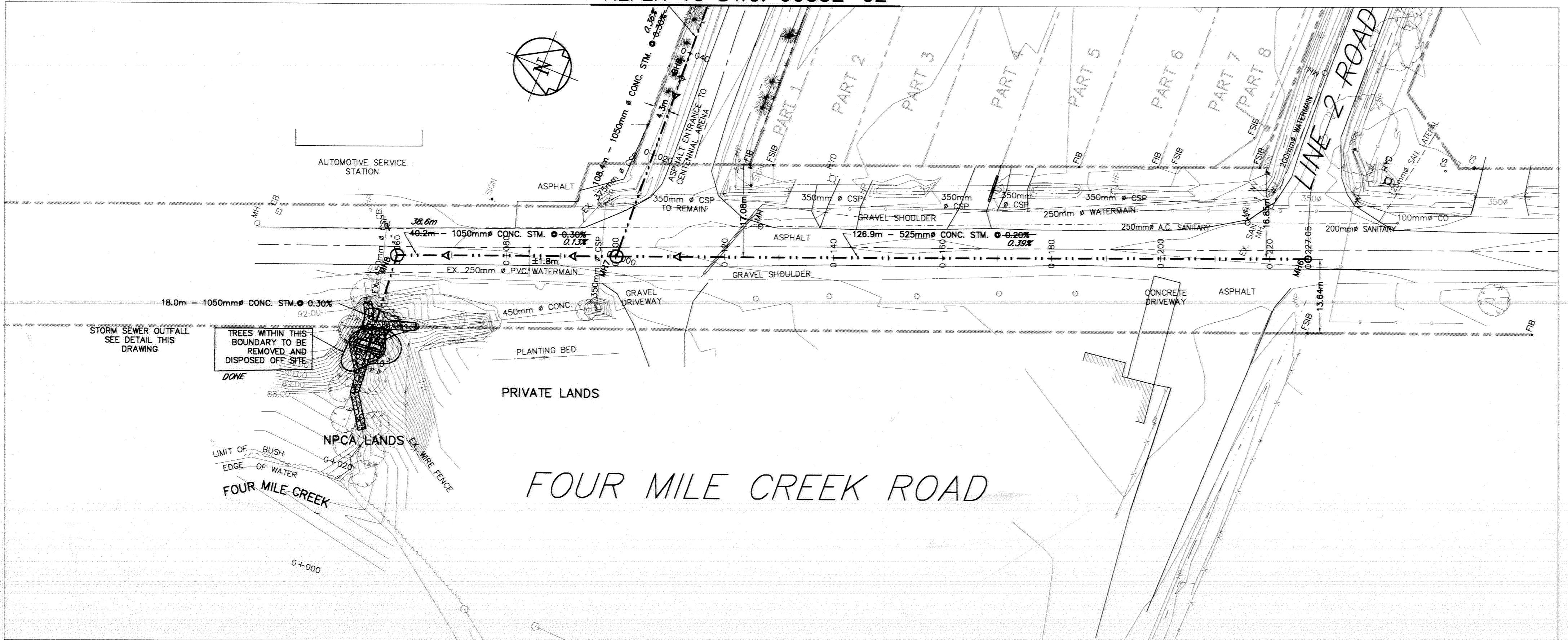
DESIGNED BY DRAWN BY CHECKED BY
W.J.F. J. DAY

SCALE H.R. 1'=40' V.R. 1'=10' DATE NOV. 1974

PROJECT NO. JOB NO. SHEET

I-0265/71 7411 7

REFER TO DWG. 99532-02



| ISSUED FOR CONSTRUCTION RECORD | 14 MAR 01 | APM |
|--------------------------------|-----------|----------|
| ISSUED FOR CONSTRUCTION | 07 MAR 00 | SEN |
| ISSUED FOR TENDER | 27 JAN 00 | HEK |
| ISSUED FOR APPROVAL | 14 JAN 00 | SEN |
| ISSUED FOR TOWN REVIEW | 10 JAN 00 | SEN |
| REVISION | DATE | INITIALS |

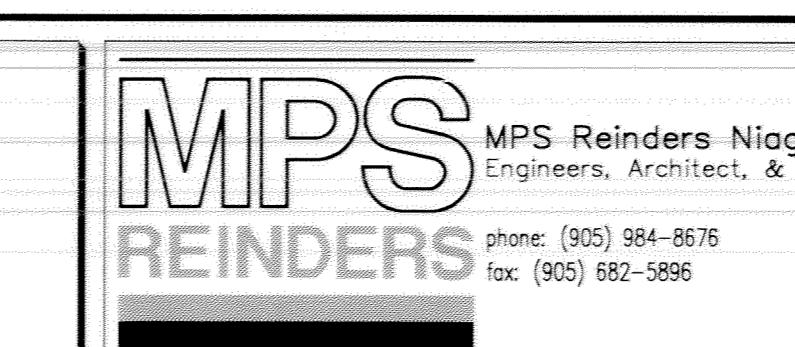
cad file:
99532-AB

NOTE:
FOR STORMWATER MANAGEMENT POND DETAILS REFER TO DWG. 99532-D1.

FOR PARK/POND/PRIVATE LAND STORM SEWER ALIGNMENT INFORMATION
REFER TO DRAWING 99532-02

THIS DRAWING IS THE COPYRIGHT
OF MPS REINDERS NIAGARA INC.
AND SHALL NOT BE MODIFIED OR
USED FOR THE ADDITIONS OR
ALTERATIONS TO THE PROJECT OR
FOR ANY OTHER PROJECT, WITHOUT
THE EXPRESSED WRITTEN CONSENT OF
MPS REINDERS NIAGARA INC.

by
N.
by
N./D.K.P.
d by
P.
AN 00



**OUTLET STORM SEWER
FOUR MILE CREEK ROAD
STA 0+000 TO
STA 0+240**

project title

scale

**LINE 2 / CONCESSION 4
DEVELOPMENT AREA
STORMWATER
MANAGEMENT**

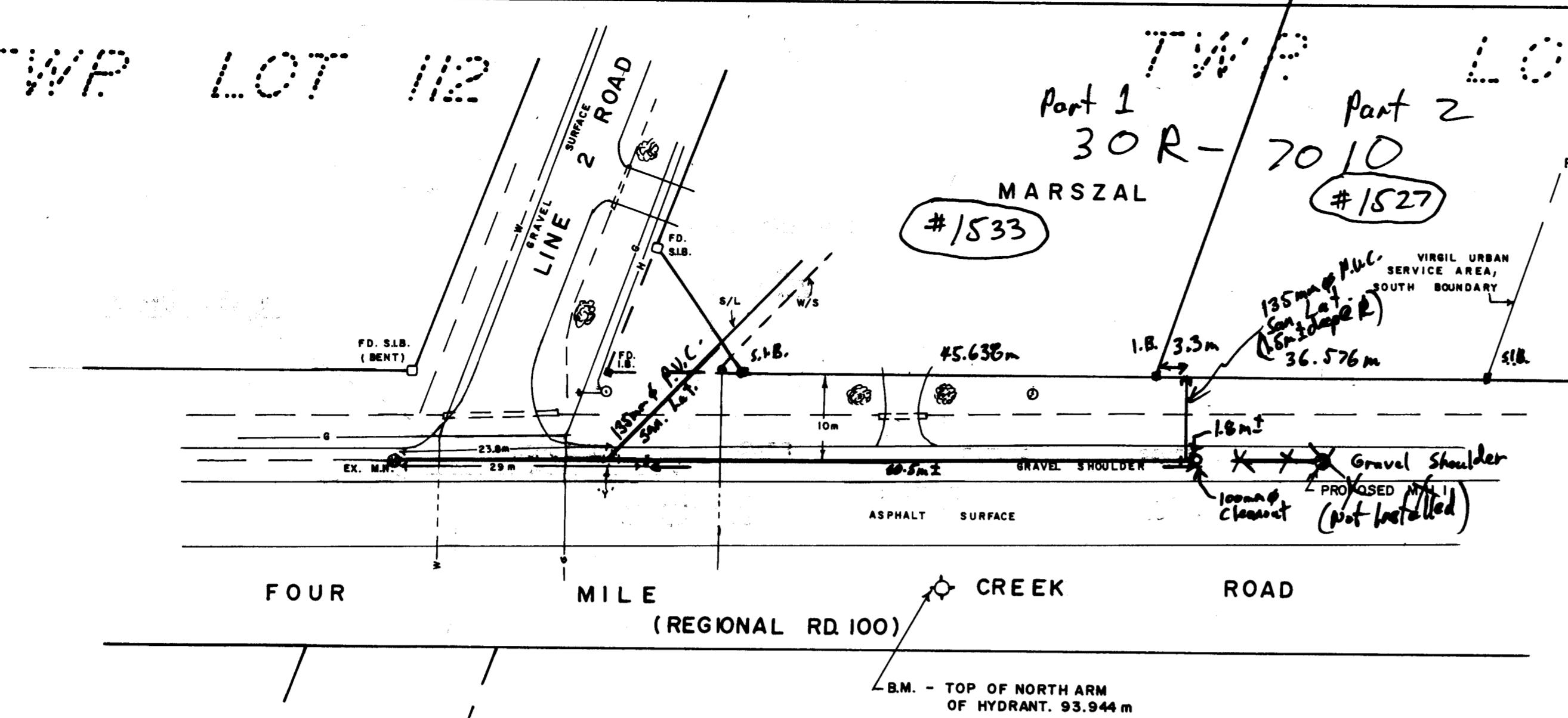
job #

99

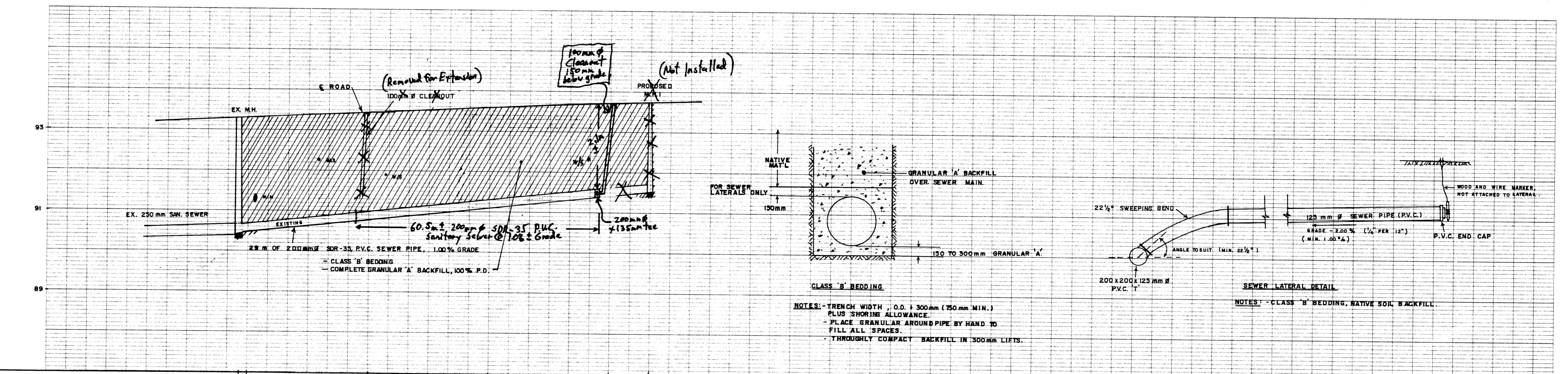
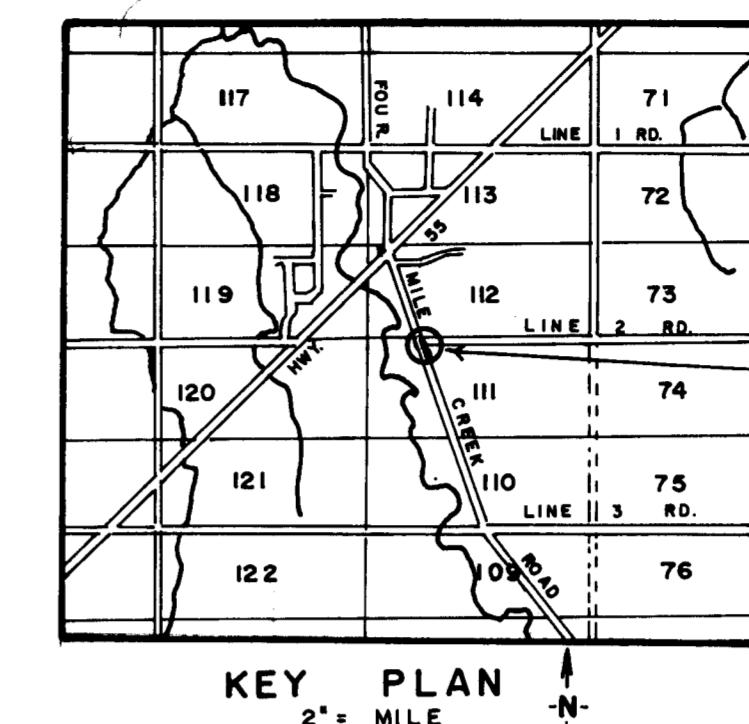
drawing

1: 500
1: 50
revision #
1
number
99532-01

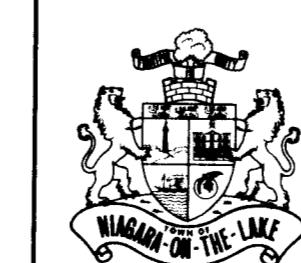
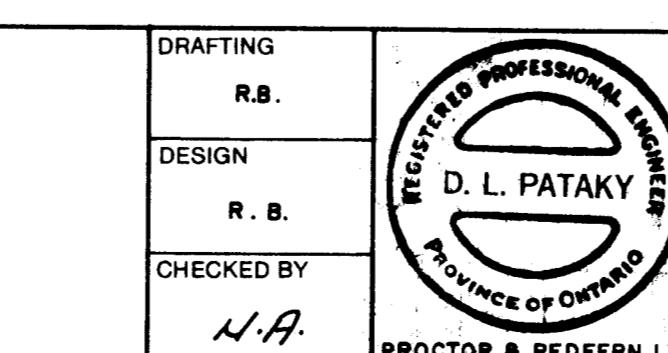
TWP LOT 112



TWP LOT 111



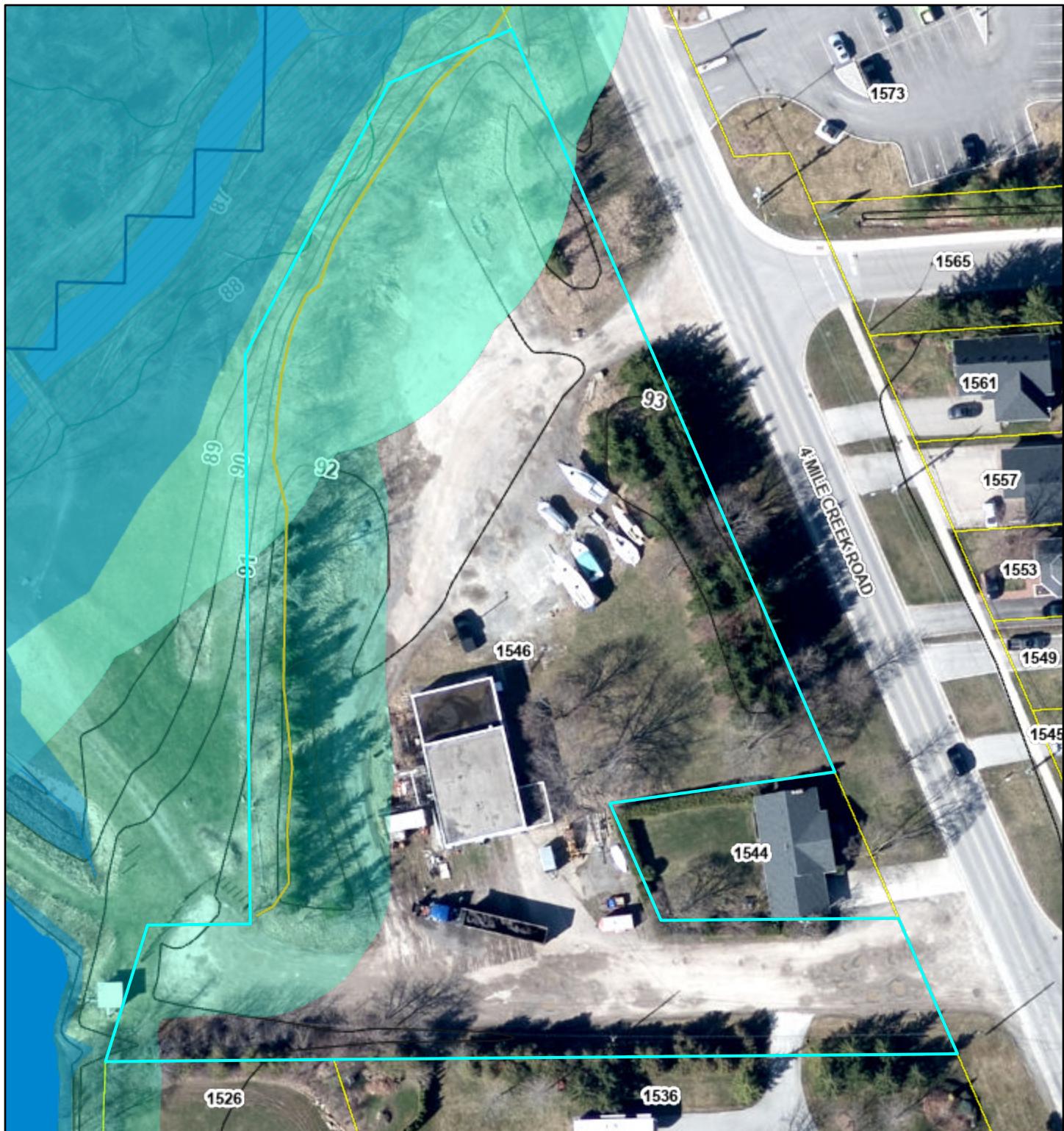
| | | | | |
|-----------------|--|-----------------|---------|-------------|
| SANITARY INVERT | S. 90.39' | | | |
| | N. 90.42 | 90.76 | 91.06 | 91.36 91.46 |
| ROAD | 93.32 | | 93.56 | |
| STATION | 2000.00 | 2000.00 | 2000.00 | 2000.00 |
| NO. | 2 As constructed, 60.5m ext. & Cleanout (7b) | 1992 06 22 L.R. | | |
| REVISION | I AS CONSTRUCTED, 29m EXT. & CLEANOUT (7a) | 1983 10 21 R.B. | | |
| DATE | | | | |
| INIT. | | | | |



TOWN OF
NIAGARA-ON-THE-LAKE
ENGINEERING DEPARTMENT

SANITARY SEWER EXTENSION
FOUR MILE CREEK RD. AT LINE 2 RD.
FIELD NOTES R.B.
DATE 1983 08 04
SCALE HOR. 1:500
VER. 1:50
DWG. NO. I OF I
MUN. REF. NO. L - 2 - 67
REV. 0

1544 & 1546 Four Mile Creek Road - Regulated Features Map



12/15/2023, 11:23:02 AM

1:1,128

SWOOP 2020 NPCA

- Red: Band_1
- Green: Band_2
- Blue: Band_3

Roads

NPCA APPROXIMATE REGULATION LANDS

Top of Slope Features

Unstable

Regulated Floodplain Extent

Regulated

0 0.01 0.01 0.02 0.02 mi
0 0.01 0.02 0.03 0.04 km

NPCA Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCan, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

From: Nicholas Bradley <nbradley@npca.ca>
Sent: Thursday, October 17, 2024 12:04 PM
To: Roshawn Nunes
Subject: 1544 & 1546 Four Mile Creek Road
Attachments: [1544 & 1546 Four Mile Creek Road - Regulated Features Map.pdf](#)

You don't often get email from nbradley@npca.ca. [Learn why this is important](#)



CAUTION: This email originated from outside of the organization. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Good afternoon,

Thank you for reaching out. The mapping of the two subject properties has been attached to this email. Please note that 1544 Four Mile Creek Road is not impacted by any NPCA regulated features. The information provided below only pertains to 1546 Four Mile Creek Road.

With reference to the attached mapping, part of 1546 Four Mile Creek Road is impacted by a Non-Provincially Significant Wetland Complex known as the Virgil Conservation Area Wetland Complex (seen in light green in the attached map). As such, new development and/or site alterations on 1546 Four Mile Creek Road would be subject to the policies under **Ontario Regulation 41/24**. Wetlands provide for natural flood attenuation during storm events and, as such, it is important to maintain the hydrologic function of wetlands to assist in minimizing flooding impacts downstream. In accordance with NPCA policies and regulations, no new development or site alterations are permitted within a wetland. Also, the NPCA uses a 30-meter buffer in which new development and site alterations may be permitted in accordance with NPCA Policies on development within the wetland buffer.

Additionally, given the topography of 1546 Four Mile Creek Road, the west side of the property would be subject to the NPCA's Valleyland Policies. The NPCA regulates all development and site alterations within 15 meters of a steep riverine valley for slope stability purposes. In accordance with current NPCA policies, new buildings and structures, accessory buildings and additions to existing buildings and structures shall provide an appropriate setback from the stable top of slope to ensure the long-term stability of the valley slope and safety of buildings or structures. This setback shall be based on a geotechnical study, approved by the NPCA. In no case shall any portion of a building or structure extend beyond the physical or stable top of slope (whichever is more restrictive).

Further, the Four Mile Creek flows adjacent to 1546 Four Mile Creek Road. This creek has an associated 1-in-100-year floodplain (seen in blue in the attached map). Current NPCA policies prohibit the placement of new structural development or fill within riverine floodplain areas. The regulatory floodplain elevation for this section of the creek is 88.78m CGVD28:78 on the north side of the property and 90.22m CGVD28:78 on the south side of the subject property. All new structures and site alterations must take place above these respective elevations to be located outside of the riverine flood hazard.

Finally, any work that encroaches on the areas of the properties that have regulated features, would fall within the jurisdiction of the NPCA and be subject to the policies under O. Reg. 41/24. Following the permitting process, applicable policies and fees would apply. Please note that depending on the scope, nature, and location of any proposed works, further supporting studies and/or plans may be required.

Thank you,
Nick



Nicholas Bradley
Planning Technician

Niagara Peninsula Conservation Authority (NPCA)
3350 Merrittville Highway, Unit 9, Thorold, Ontario L2V 4Y6

905.788.3135 ext. 279
www.nPCA.ca
nbradley@nPCA.ca

The information contained in this communication, including any attachment(s), may be confidential, is intended only for the use of the recipient(s) named above. If the reader of this message is not the intended recipient, you are hereby notified that any disclosure of this communication, or any of its contents, is prohibited. If you have received this communication in error, please notify the sender and permanently delete the original and any copy from your computer system. Thank-you. Niagara Peninsula Conservation Authority.

Appendix B – Existing Conditions Calculations

Pre-Development Runoff Coefficients and Peak Flows

Town of Niagara on the Lake

| Contributing Area | ID# | Runoff Coefficient | AREA (ha) |
|-------------------|-----|--------------------|-----------|
| Cathcment 1 | 101 | 0.43 | 0.65 |
| Cathcment 2 | 102 | 0.25 | 0.07 |
| Cathcment 3 | 103 | 0.55 | 0.35 |
| TOTAL | | 0.46 | 1.07 |

Pre-Development Flows Catchment 101

| | | | |
|-----------------------|--------------|--------------------------------------|-----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 57.8 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5 \text{ Year})} = C*I*A/360$ | 69.8 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100 \text{ Year})} = C*I*A/360$ | 112.0 l/s |

Pre-Development Flows Catchment 102

| | | | |
|-----------------------|--------------|--------------------------------------|---------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 3.6 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5 \text{ Year})} = C*I*A/360$ | 4.4 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100 \text{ Year})} = C*I*A/360$ | 7.0 l/s |

Pre-Development Flows Catchment 103

| | | | |
|-----------------------|--------------|--------------------------------------|----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 39.8 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5 \text{ Year})} = C*I*A/360$ | 48.1 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100 \text{ Year})} = C*I*A/360$ | 77.1 l/s |

Appendix C – Proposed Conditions Calculations

Post-Development Runoff Coefficients and Peak Flows

Town of Niagara on the Lake

| Contributing Area | ID# | Runoff Coefficient | AREA (ha) |
|-------------------|-----|--------------------|-------------|
| Catchment 1 | 201 | 0.82 | 0.53 |
| Catchment 2 | 202 | 0.95 | 0.17 |
| Catchment 3 | 203 | 0.80 | 0.26 |
| Catchment 4 | 204 | 0.25 | 0.11 |
| TOTAL | | 0.78 | 1.07 |

Post-Development Flows Catchment 201

| | | | |
|-----------------------|--------------|------------------------------------|-----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 89.9 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5\text{Year})} = C*I*A/360$ | 108.5 l/s |
| 10 Year Intensity | 101.38 mm/hr | $Q_{(10\text{Year})} = C*I*A/360$ | 122.4 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100\text{Year})} = C*I*A/360$ | 174.2 l/s |

Post-Development Flows Catchment 202

| | | | |
|-----------------------|--------------|------------------------------------|----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 33.4 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5\text{Year})} = C*I*A/360$ | 40.3 l/s |
| 10 Year Intensity | 101.38 mm/hr | $Q_{(10\text{Year})} = C*I*A/360$ | 45.5 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100\text{Year})} = C*I*A/360$ | 64.7 l/s |

Post-Development Flows Catchment 203

| | | | |
|-----------------------|--------------|------------------------------------|----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 43.0 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5\text{Year})} = C*I*A/360$ | 51.9 l/s |
| 10 Year Intensity | 101.38 mm/hr | $Q_{(10\text{Year})} = C*I*A/360$ | 58.6 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100\text{Year})} = C*I*A/360$ | 83.4 l/s |

Post-Development Flows Catchment 204

| | | | |
|-----------------------|--------------|------------------------------------|----------|
| Time of Concentration | 10 minutes | | |
| 2 Year Intensity | 74.46 mm/hr | $Q_{(2\text{Year})} = C*I*A/360$ | 5.7 l/s |
| 5 Year Intensity | 89.88 mm/hr | $Q_{(5\text{Year})} = C*I*A/360$ | 6.9 l/s |
| 10 Year Intensity | 101.38 mm/hr | $Q_{(10\text{Year})} = C*I*A/360$ | 7.7 l/s |
| 100 Year Intensity | 144.26 mm/hr | $Q_{(100\text{Year})} = C*I*A/360$ | 11.0 l/s |

Catchment Area 201

Required Storage Volume

Town of Niagara on the Lake

Control 100 year Post Development to 5 Year Pre Development

Controlled Site Area 5300 m²

Allowable Release From Site 42.22 l/s

Orifice Control 41.4 l/s

Composite Runoff Coefficient (Controlled Area) 0.82

Time of Concentration 10 minutes

100 Year Storm I = 980/(t+3.7)^{0.732}

| Storm Duration (minutes) | Rainfall Intensity (mm/hr) | Total Runoff Q (l/s) | Required Storage Volume (m ³) |
|--|----------------------------|----------------------|---|
| 2 | 274.111 | 330.9 | 34.7 |
| 4 | 219.945 | 265.5 | 53.8 |
| 6 | 185.742 | 224.2 | 65.8 |
| 8 | 161.925 | 195.5 | 74.0 |
| 10 | 144.260 | 174.2 | 79.7 |
| 12 | 130.565 | 157.6 | 83.7 |
| 14 | 119.594 | 144.4 | 86.5 |
| 16 | 110.580 | 133.5 | 88.4 |
| 18 | 103.024 | 124.4 | 89.6 |
| 20 | 96.585 | 116.6 | 90.2 |
| 22 | 91.024 | 109.9 | 90.4 |
| 24 | 86.165 | 104.0 | 90.2 |
| 26 | 81.878 | 98.8 | 89.6 |
| 28 | 78.064 | 94.2 | 88.8 |
| 30 | 74.645 | 90.1 | 87.7 |
| 32 | 71.560 | 86.4 | 86.4 |
| 34 | 68.761 | 83.0 | 84.9 |
| 36 | 66.208 | 79.9 | 83.2 |
| 38 | 63.868 | 77.1 | 81.4 |
| 40 | 61.715 | 74.5 | 79.5 |
| 90 m³ of Storage is required | | | |

100 YEAR STORM EVENT- SWM Controls

PROJECT: 1544 & 1546 Four Mile Creek Road

PROJECT No: ALL-24011473-A0

CREATED: 26-Feb-25

PRINTED: 26-Feb-25

INPUT

| | |
|--------------------------------|--------|
| Net Required Discharge (l/s) = | 174.20 |
| Max. Water Surface Elev. (m) = | 92.80 |
| Discharge Pipe Invert (m) = | 90.64 |
| Discharge Pipe Diameter (mm) = | 300 |
| Orifice Diameter (mm) = | 100 |
| Orifice Flow Loss (C) = | 0.82 |

OUTPUT

$$\begin{aligned} H &= 2.11 \quad \text{m} \\ g &= 9.806 \\ V &= (2*g*H)^{0.5} = 6.433 \quad \text{m/s} \\ A &= \text{X-section Area} = 0.0079 \quad \text{m}^2 \end{aligned}$$

| | | |
|---------------------------------------|------|-----|
| Orifice Flow = Q = C * A * V * 1000 = | 41.4 | l/s |
|---------------------------------------|------|-----|

Cathment Area 202 + 203

Required Storage Volume

Town of Niagara on the Lake

Control 100 year Post Development to 5 Year Pre Development

| | |
|--|---------------------|
| Controlled Site Area | 4300 m ² |
| Allowable Release From Site | 22.73 l/s |
| Orifice Control | 22 l/s |
| Composite Runoff Coefficient (Controlled Area) | 0.65 |
| Time of Concentration | 10 minutes |

$$100 \text{ Year Storm } I = 980/(t+3.7)^{0.732}$$

| Storm Duration (minutes) | Rainfall Intensity (mm/hr) | Total Runoff Q (l/s) | Required Storage Volume (m ³) |
|--|----------------------------|----------------------|---|
| 2 | 274.111 | 212.8 | 22.9 |
| 4 | 219.945 | 170.8 | 35.7 |
| 6 | 185.742 | 144.2 | 44.0 |
| 8 | 161.925 | 125.7 | 49.8 |
| 10 | 144.260 | 112.0 | 54.0 |
| 12 | 130.565 | 101.4 | 57.1 |
| 14 | 119.594 | 92.9 | 59.5 |
| 16 | 110.580 | 85.9 | 61.3 |
| 18 | 103.024 | 80.0 | 62.6 |
| 20 | 96.585 | 75.0 | 63.6 |
| 22 | 91.024 | 70.7 | 64.2 |
| 24 | 86.165 | 66.9 | 64.7 |
| 26 | 81.878 | 63.6 | 64.8 |
| 28 | 78.064 | 60.6 | 64.9 |
| 30 | 74.645 | 58.0 | 64.7 |
| 32 | 71.560 | 55.6 | 64.4 |
| 34 | 68.761 | 53.4 | 64.0 |
| 36 | 66.208 | 51.4 | 63.5 |
| 38 | 63.868 | 49.6 | 62.9 |
| 40 | 61.715 | 47.9 | 62.2 |
| 65 m³ of Storage is required | | | |

100 YEAR STORM EVENT- SWM Controls

PROJECT: 1544 & 1546 Four Mile Creek Road

PROJECT No: ALL-24011473-A0

CREATED: 26-Feb-25

PRINTED: 26-Feb-25

INPUT

| | |
|--------------------------------|--------|
| Net Required Discharge (l/s) = | 148.10 |
| Max. Water Surface Elev. (m) = | 92.30 |
| Discharge Pipe Invert (m) = | 91.12 |
| Discharge Pipe Diameter (mm) = | 300 |
| Orifice Diameter (mm) = | 85 |
| Orifice Flow Loss (C) = | 0.82 |

OUTPUT

$$\begin{aligned} H &= 1.1375 \quad \text{m} \\ g &= 9.806 \\ V &= (2*g*H)^{0.5} = 4.723 \quad \text{m/s} \\ A &= \text{X-section Area} = 0.0057 \quad \text{m}^2 \end{aligned}$$

Orifice Flow = Q = C * A * V * 1000 = 22.0 l/s

End of Document

